

# Comparing Seasonal Forecasts of Industrial Production

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# COMPARING SEASONAL FORECASTS OF INDUSTRIAL PRODUCTION\*

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## Abstract

Forecast combination methodologies exploit complementary relations between different types of econometric models. The development and growing use of such combinations results from the fact that this approach often delivers more accurate forecasts than the individual models on which these forecasts are based. This paper examines forecasts of seasonally unadjusted monthly industrial production data for 17 countries and the Euro Area, comparing individual model forecasts and forecast combination methods in order to examine whether the latter are able to take advantage of the properties of different seasonal specifications. In addition to linear models (with deterministic seasonality and with nonstationary stochastic seasonality), more complex models that capture deterministic nonlinearity (periodic autoregressions) or stochastic nonlinearity (self-exciting threshold autoregressive nonlinear models) are also examined. Forecast combinations consistently provide the best performance at short horizons, implying that utilizing the different characteristics captured by these models can contribute to improved forecast accuracy. Although periodic models perform relative well, nonlinear models perform poorly.

**Key words:** Forecast combinations, seasonality, RMSPE, Periodic models, SETAR models.

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## 1. Introduction

Agents working with seasonal data often require forecasts of intra-year observations; for example, managers need to forecast future monthly demand for their products in order to ensure that they have sufficient stocks on hand to meet this demand. Indeed, the production of many commodities is itself highly seasonal, largely due to the traditional factory closures that take place during the summer and Christmas periods. Perhaps because of their marked intra-year patterns, economists interested in seasonality have often focused on industrial production series (for example, Beaulieu and Miron, 1991, Cecchetti and Kashyap, 1996, Matas-Mir and Osborn, 2004).

The nature of seasonality is also of interest to official statistical agencies, including EuroStat, which is responsible for data provision relating to the European Union. Although many economists concentrate on seasonally adjusted values, the process of seasonal adjustment may itself involve forecasting future intra-year values of the unadjusted series, as discussed by Ghysels, Osborn and Rodrigues (2006) in the context of the recently-developed X-12-ARIMA method of the US Bureau of the Census. There has, however, been surprisingly little empirical analysis of the accuracy of methods for forecasting seasonal economic time series.

Rather than selecting a single model for forecasting, an alternative approach is to combine forecasts derived from a range of models. This has particular attractions in the context of forecasting seasonal series, since there are a number of different ways of handling seasonality that may be appropriate depending on the properties of the series in question. For example, the seasonality may be of the deterministic form, it may exhibit nonstationary stochastic properties, it may be periodic (seasonally-varying coefficient) in nature, or it may exhibit non-linear interaction with the business cycle; see Ghysels and Osborn (2001) for discussion of some relevant models and their properties. Rather than choosing between these possibilities, a user may elect to adopt a forecast based on a combination of models. Indeed, the use of a suitably chosen combination may lead to improved forecast accuracy compared to the choice of a single method.

Since the early work of Bates and Granger (1969), several methods have been developed for combining forecasts. Since time series models are simplifications of complicated processes that are imperfectly understood, single models are typically incomplete representations of a data generation process (DGP). Hence, combinations of forecasts from different models, which may provide complementary information about the DGP, can assist in the approximation of the DGP. In practice, such combinations are often found to outperform forecasts produced by a single model (see, *inter alia*, Bates and Granger, 1969, Granger and Ramanathan, 1984, Stock and Watson, 1999). Against this, Hibon and Evgeniou (2005) find that the best individual forecast model performs as well as the best combination. Nevertheless, as these authors state, combining forecasts retains an advantage in being less risky than selecting among the available individual model forecasts.

This paper studies the post-sample accuracy of forecasts of seasonally unadjusted monthly industrial production indices (IPI) from 17 individual countries (Austria, Canada, Denmark, Finland, France, Germany, Greece, Hungary, Italy, Japan, Luxembourg, Netherlands, Portugal, Spain, Sweden, United Kingdom and USA) and an aggregate series for the Euro Area.

In total, we examine 17 (linear and nonlinear) forecasting models and 18 procedures for combining the information from these 17 models. Our aim is to examine the relative accuracy of these approaches and to investigate whether any general lessons emerge about whether combining forecasts improves accuracy for these series.

The outline of the paper is as follows. Section 2 briefly introduces the forecast models considered in this paper. In Section 3 we study the empirical properties of the IPI series, *i.e.*, we investigate whether the IPI series display seasonal non-stationarity, non-linearity and periodicity (seasonally-varying coefficients). Section 4 discusses predictive accuracy measures and introduces the combination methods considered. The substantive results in relation to forecast accuracy for the seasonal IPI series are contained in Section 5. Finally, Section 6 concludes the paper.

## 2. The Models

This section briefly presents the seasonal models that are later applied in forecasting. In line with Ghysels, Osborn and Rodrigues (2006), we first discuss representations of seasonality in the context of constant parameter linear models, with subsequent subsections considering non-linear (SETAR) and periodic models. Although most of this discussion is general in the sense of referring to  $S$  seasons per year, our empirical analysis of monthly IPI below (obviously) employs  $S = 12$ .

### 2.1. Linear Seasonal Models

For the purpose of presentation, consider the model

$$y_{Sn+s} = \mu_{Sn+s} + x_{Sn+s} \quad (2.1)$$

$$\phi(L)x_{Sn+s} = u_{Sn+s} \quad (2.2)$$

where  $y_{Sn+s}$  ( $s = 1, \dots, S, n = 0, \dots, T - 1$ ) represents the observed value in season  $s$  (in our application this is a month) of year  $n$ , the polynomial  $\phi(L)$  contains any unit roots in  $y_{Sn+s}$  and is specified in the following subsections according to the model being discussed,  $L$  represents the conventional lag operator,  $L^k x_{Sn+s} \equiv x_{Sn+s-k}$ ,  $k = 0, 1, \dots$ , the driving shocks  $\{u_{Sn+s}\}$  of (2.2) are assumed to follow an ARMA( $p, q$ ),  $0 \leq p, q < \infty$  process, such as,  $\beta(L)u_{Sn+s} = \theta(L)\varepsilon_{Sn+s}$ , where the roots of  $\beta(z) \equiv 1 - \sum_{j=1}^p \beta_j z^j = 0$  and  $\theta(z) \equiv 1 - \sum_{v=1}^q \theta_v z^v = 0$  lie outside the unit circle,  $|z| = 1$  and  $\varepsilon_{Sn+s} \sim iid(0, \sigma^2)$ . The term  $\mu_{Sn+s}$  represents a deterministic kernel which is assumed to be either i) a set of seasonal means, *i.e.*,  $\sum_{s=1}^S \delta_s D_{s,Sn+s}$  where  $D_{s,Sn+s}$  is a dummy variable taking value 1 in season  $s$  and zero elsewhere, or ii) a set of seasonals with a (nonseasonal) time trend, *i.e.*,  $\sum_{s=1}^S \delta_s D_{s,Sn+s} + \tau(Sn + s)$ . In general, the second of these is more plausible for economic time series, since it allows the underlying level of the series to trend over time, whereas  $\mu_{Sn+s} = \delta_s$  implies a constant underlying level, except for seasonal variation.

Linear forecasting models can be classified in terms of their assumptions about unit roots in  $\phi(L)$ . The two most common forms of seasonal models in empirical economics employ

seasonally integrated models, with  $\phi(L) = \Delta_S$  in (2.2), or deterministic seasonality with either  $\phi(L) = 1 - L$  or  $\phi(L) = 1$ . In addition, seasonal autoregressive integrated moving average (SARIMA) models with  $\phi(L) = \Delta_S \Delta$  retain an important role as a forecasting benchmark. Each of these three models is briefly discussed in a separate subsection below.

### 2.1.1. Seasonally Integrated Model

The seasonally integrated model assumes that seasonality is nonstationary, with seasonal (or annual) differencing of  $y_{Sn+s}$  required in order to render the process stationary. This implies that  $\phi(L) = 1 - L^S = \Delta_S$  in (2.1) and, since  $\Delta_S = (1 - L)(1 + L + L^2 + \dots + L^{S-1})$ , seasonal integration imposes the presence of unit roots not only at the zero frequency, but also at each of the so-called seasonal frequencies.

Stationary dynamics in economic time series are often represented as being of the autoregressive (AR) form. With this assumption, namely  $\beta(L)u_{Sn+s} = \varepsilon_{Sn+s}$  in (2.2), the seasonally integrated model is

$$\beta(L)\Delta_S y_{Sn+s} = \beta(1)S\tau + \varepsilon_{Sn+s} \quad (2.3)$$

since  $\Delta_S \mu_{Sn+s} = S\tau$ . Thus, with the inclusion of an intercept, the seasonally integrated process of (2.3) has a common annual drift,  $\beta(1)S\tau$ , across seasons. Clearly, the essential features of the model are retained if a moving average component is added to (2.3). Notice that the underlying seasonal means  $\mu_{Sn+s}$  are not observed, since the seasonally varying component  $\sum_{s=1}^S \delta_s D_{s,Sn+s}$  of  $\mu_{Sn+s}$  in (2.1) is annihilated by seasonal (that is, annual) differencing.

From an economic point of view, nonstationary seasonality can be controversial because the values over different seasons are not cointegrated and hence can move in any direction in relation to each other, so that “*winter can become summer*”. This lack of cointegration appears to have been first noted by Osborn (1991). Prior to using a seasonally integrated model, tests can be conducted to investigate the validity of the unit root assumption, with the most popular approach to testing for seasonal integration being that of Hylleberg, Engle, Granger and Yoo [HEGY] (1990).

### 2.1.2. Deterministic Seasonal Models

When seasonality results in peaks and troughs within a particular season, year after year, it can be described by deterministic variables leading to what is conventionally referred to as *deterministic seasonality*. In this case the underlying seasonal pattern is assumed to display means that are constant over time.

A simple deterministic seasonal model can permit with stationary AR dynamics, with

$$\beta(L)y_{Sn+s} = \sum_{s=1}^S \beta(L)[\delta_s D_{s,Sn+s}] + \beta(1)(Sn + s)\tau + \varepsilon_{Sn+s} \quad (2.4)$$

where  $\varepsilon_{Sn+s}$  is again a zero mean white noise process, and  $\beta(L)$  is a  $p$ th order polynomial. In this case, the deterministic component of the estimated model explicitly includes seasonal

intercepts and a linear trend. However, the assumption of stationary dynamics may be unrealistic since it is common for economic time series to exhibit evidence of a zero frequency unit root. Therefore,  $\phi(L) = 1 - L$  may be imposed in (2.2). Again assuming that the stationary dynamics are of the AR form, (2.1)-(2.2) then becomes

$$\beta(L)\Delta_1 y_{S_n+s} = \sum_{s=1}^S \beta(L)\Delta_1 \mu_{S_n+s} + \varepsilon_{S_n+s} \quad (2.5)$$

where  $\Delta_1 \mu_{S_n+s} = \mu_{S_n+s} - \mu_{S_{n+s-1}}$ , so that (only) the change in the seasonal means between seasons  $s$  and  $s-1$  is identified.

### 2.1.3. SARIMA Model

When working with nonstationary seasonal data, both annual changes and changes between adjacent seasons are important concepts. This motivated the model

$$\beta(L)(1-L)(1-L^S)y_{S_n+s} = \theta(L)\varepsilon_{S_n+s} \quad (2.6)$$

which results from specifying  $\phi(L) = \Delta_1 \Delta_S = (1-L)(1-L^S)$  in (2.2). The intuition is that the filter  $(1-L^S)$  captures the tendency for the value of the series for a particular season to be highly correlated with the value for the same season a year earlier, while  $(1-L)$  captures the nonstationary nonseasonal stochastic component. It is worth noting that the imposition of  $\Delta_1 \Delta_S$  annihilates the deterministic variables (seasonal means and time trend) of (2.1), so that these do not appear in (2.6).

However, since  $(1-L)(1-L^S) = (1-L)^2(1+L+L^2+\dots+L^{S-1})$ , (2.6) imposes unit roots at all seasonal frequencies, as well as two unit roots at the zero frequency. As a result these models may be empirically implausible (see *e.g.* Osborn, 1990 and Helleberg, Jørgensen and Sørensen, 1993). Nevertheless, they can be successful in forecasting due to their parsimonious nature and hence may provide a benchmark for forecast accuracy comparisons.

A specific SARIMA model of particular interest in seasonal modelling is the widely used "airline model", which imposes  $\beta(L) = 1$  in (2.6), together with  $\theta(L) = (1-\theta L)(1-\Theta L^S)$ .

## 2.2. Seasonal SETAR Models

SETAR models are a class of model particularly suited for modelling of economic variables with asymmetric behaviour, since these allow for the classification of observations into different regimes according to the value taken by a specific threshold variable.

In this study, we consider a seasonal two-regime, seasonal SETAR (*SSETAR*) model of order  $p$  of the form

$$y_{S_n+s} = \sum_{k=1}^2 \sum_{s=1}^S [\lambda_s D_{s,S_n+s} + \delta_s D_{s,S_n+s}(S_n+s)] I_{k,S_n+s} + \sum_{i=1}^p \rho_i y_{S_n+s-i} + \varepsilon_t \quad (2.7)$$

with  $s = 1, 2, \dots, S$  and where  $D_{s,S_n+s}$  represents the usual seasonal dummy variable for season  $s$ ,  $I_{k,S_n+s}$  corresponds to an indicator variable determined by  $q_{S_n+s-d}$ ,  $q_{S_n+s-d}$  is a

threshold variable and  $d$  is a delay parameter; the disturbance in each regime is assumed to be white noise. The regimes in (2.7) are defined by the value of  $q_{Sn+s}$  in relation to some threshold  $\gamma$ . In practice the threshold variable typically employs a lag of  $y_{Sn+s}$ , or a linear combination of lagged  $y_{Sn+s}$ ; see, *inter alia*, Tsay (1989, p.23) and Hansen (1997, p.10). Notice that (2.7) allows only the intercept to vary over time, with the AR lag coefficients assumed to be invariant to the season and the regime. Although more general forms of SSETAR model can be employed, their greater flexibility implies the estimation of a larger number of coefficients. In our forecasting context, we prefer the more parsimonious version of (2.7).

Implicitly (2.7) assumes that  $y_{Sn+s}$  is stationary. To allow for unit root behavior, (2.7) may be estimated using  $\Delta_1 y_{Sn+s}$ ; see Matas-Mir and Osborn (2004).

However, before this type of model is applied in empirical work, it is important to determine whether the data justifies its use through a test for threshold effects. Chan and Tong (1990) and Hansen (1997) suggest the following test statistic,

$$F(\gamma) = n \left( \frac{\tilde{\sigma}^2 - \hat{\sigma}^2(\gamma)}{\hat{\sigma}^2(\gamma)} \right) \quad (2.8)$$

where  $\tilde{\sigma}^2$  and  $\hat{\sigma}^2(\gamma)$  represent the variance estimators acquired from the residuals of a linear and a SETAR model, respectively. The null hypothesis considers a linear model as appropriate, while the alternative of regime-dependent coefficients supports the SETAR model.

However, a difficulty in applying these tests for threshold effects relates to the presence of the nuisance parameter,  $\gamma$ , under the alternative hypothesis only. This problem, was first identified by Davis (1977) and invalidates the use of conventional asymptotic theory when the threshold effect,  $\gamma$ , is unknown; see also Andrews and Ploberger (1994) and Hansen (1996). In this case, critical values for (2.8) can be obtained using the bootstrap method as suggested by Hansen (1997, 2000).

### 2.3. Periodic Models

Periodic autoregressive (PAR) models provide another class of model for seasonally unadjusted data, where these models allow coefficients to change according to the seasons of a year. This seasonal parameter variation can prove useful in describing economic situations in which choices made by economic agents show distinct seasonal characteristics. Problems associated with dismissing periodicity are well described in Osborn (1991) and in Tiao and Grupe (1980).

PAR models assume that the observations for different seasons can be described by distinct autoregressive models. We consider the following PAR( $S, p$ ) model

$$y_{Sn+s} = \sum_{s=1}^S [\lambda_s D_{s,Sn+s} + \delta_s D_{s,Sn+s}(Sn+s)] + \sum_{s=1}^S \sum_{j=1}^{p_s} \alpha_{js} D_{s,Sn+s} y_{Sn+s-j} + \varepsilon_{Sn+s} \quad (2.9)$$

where  $S$  represents the periodicity of the data,  $p_s$  the order of the autoregressive component corresponding to season  $s$ ,  $p = \max(p_1, \dots, p_S)$ ,  $\varepsilon_{Sn+s} \sim iid(0, \sigma^2)$  and  $D_{s,Sn+s}$  a seasonal dummy equal to 1 in season  $s$  and zero otherwise; see for instance Clements and Smith

(1997). In its unrestricted form of (2.9), the model coefficients can be estimated by ordinary least squares.

PAR models can be applied to either the levels of the series, as in (2.9), or after the application of first differences.

Similarly to the SETAR models previously discussed, it is also advisable in this case to first verify whether the data shows this type of properties before employing them in a forecasting model. There are different approaches available in the literature when testing for the presence of periodicity. The most direct is to consider the null non-periodic hypothesis

$$H_0 : \alpha_{is} = \alpha_i, \quad s = 1, \dots, S, i = 1, \dots, p \quad (2.10)$$

against the alternative that not all  $\alpha_{is}$  are equal, which we denote as  $F_{PAR}$ . This test can be performed by the usual F-test, which (for  $T$  sample observations used for estimation of (2.9)) asymptotically follows an F distribution with  $((S - 1)p, T - (S + 2)p)$  degrees of freedom; see Boswijk and Franses (1996).

Alternatively, following Franses (1996, pp.101-102) a residual-based approach can be adopted. As a first step, a non-periodic AR(p) model is estimated. Using the resulting residuals, periodicity is tested through the auxiliary regression,

$$\hat{v}_{Sn+s} = \sum_{i=1}^p \phi_i y_{Sn+s-i} + \sum_{j=1}^r \sum_{s=1}^S \gamma_{js} D_{s,Sn+s} \hat{v}_{Sn+s-j} + u_{Sn+s} \quad (2.11)$$

via an F-test for the joint significance of the  $\gamma_{js}$  for some order of autocorrelation  $r$ . Under the non-periodic null hypothesis, this F-statistic asymptotically follows a standard F-distribution with  $(Sr, T - p - Sr)$  degrees of freedom. As an alternative option or a complementary procedure, the auxiliary regression

$$\hat{v}_{Sn+s}^2 = \omega_0 + \sum_{k=1}^{S-1} \omega_k D_{k,Sn+s} + e_{Sn+s} \quad (2.12)$$

can be used to check for seasonal heteroscedasticity. As argued by Franses (1996), neglected parameter variations may surface in the variance of the residual process. Thus, under the null hypothesis of no seasonal heteroscedasticity, an F-test for  $\omega_k = 0, k = 1, \dots, S - 1$  asymptotically follows a standard F-distribution with  $(S - 1, T - p)$  degrees of freedom.

It should be noted, however, that a finding of seasonal heteroscedasticity does not necessarily imply that a PAR model should be used, since this could arise from a conventional constant-coefficient model subject to disturbances which have seasonally-varying variances.

### 3. Empirical Properties of Industrial Production

#### 3.1. Data

The data used in this study is the logarithm of monthly Industrial Production data for 17 individual countries and the Euro Area. Therefore, the first difference has the interpretation of the monthly growth rate, and the annual difference as the annual growth rate. Table 3.1 reports some descriptive statistics for the annual and monthly growth rates, after outlier correction. Outlier detection and correction was carried out using the Tramo/Seats program developed by Gomez and Maravall (1996). For ease of interpretation, the differenced values are multiplied by 100 prior to the calculation of the statistics of Table 3.1.

**Table 3.1: Descriptive Statistics**

| Country     |          |    |    | Annual Growth |      | Monthly Growth |       |
|-------------|----------|----|----|---------------|------|----------------|-------|
|             | Outliers |    |    | Mean          | SD   | Mean           | SD    |
|             | AO       | TC | LS |               |      |                |       |
| Austria     | 0        | 0  | 0  | 3.21          | 3.90 | 0.30           | 8.59  |
| Canada      | 0        | 1  | 0  | 2.57          | 4.87 | 0.19           | 6.25  |
| Denmark     | 0        | 2  | 0  | 2.40          | 6.55 | 0.20           | 17.16 |
| Finland     | 3        | 0  | 2  | 3.39          | 5.81 | 0.29           | 14.92 |
| France      | 0        | 0  | 1  | 1.14          | 3.15 | 0.08           | 15.13 |
| Germany     | 2        | 0  | 1  | 1.37          | 3.37 | 0.10           | 6.71  |
| Greece      | 2        | 3  | 1  | 1.09          | 4.11 | 0.09           | 8.04  |
| Hungary     | 0        | 1  | 0  | 2.52          | 8.72 | 0.25           | 10.90 |
| Italy       | 0        | 0  | 0  | 0.90          | 4.36 | 0.06           | 31.85 |
| Japan       | 0        | 0  | 0  | 1.68          | 4.91 | 0.18           | 7.53  |
| Luxembourg  | 1        | 1  | 2  | 3.29          | 6.01 | 0.24           | 12.53 |
| Netherlands | 0        | 0  | 0  | 0.99          | 4.16 | 0.07           | 7.84  |
| Portugal    | 1        | 0  | 0  | 2.44          | 4.99 | 0.18           | 15.59 |
| Spain       | 0        | 0  | 1  | 1.70          | 3.46 | 0.17           | 21.00 |
| Sweden      | 3        | 0  | 2  | 2.64          | 4.52 | 0.22           | 26.46 |
| UK          | 0        | 0  | 1  | 1.00          | 3.52 | 0.06           | 7.14  |
| USA         | 2        | 2  | 1  | 2.52          | 3.67 | 0.21           | 2.01  |
| Euro Area   | 3        | 0  | 3  | 1.55          | 3.09 | 0.12           | 11.12 |

Note: The columns labeled AO, TC and LS refer to the nature of outliers detected and indicate the respective number of outliers observed. Outlier detection and correction was carried out using the automatic procedure in TRAMO/SEATS.

Our data covers the period January 1980 to December 2005 (before differencing). However, outliers are removed only for the subsample used for the estimation of the models, *i.e.*, January 1980 to December 2002.

Although IPI growth over this period is positive in all cases, Table 3.1 indicates very different experiences across the countries considered for the mean and variability of IPI growth. For example, Italy, Spain and Sweden have a standard deviation of monthly growth

around six to eight times that of annual growth, pointing to the highly seasonal nature of these IPI series.

The remainder of this section discusses some tests undertaken to examine the characteristics of our data series. Note that the outlier corrected subsample to December 2002 is used for this analysis.

### 3.2. Seasonal Nonstationarity

In principle, the appropriate modelling of seasonality depends on whether the series is seasonally integrated or is stationary around deterministic seasonal means. Therefore, preliminary tests for seasonal nonstationarity are undertaken prior to developing a specific forecasting model.

In order to test for seasonal nonstationarity, and following Smith and Taylor (1999), expanding  $\phi(L) = \Delta_{12}$  in (2.2) around the unit roots at different frequencies (*i.e.*, zero,  $\pi$  and  $\exp(\pm i2\pi k/12)$  with  $k = 1, \dots, 5$ ), including the necessary deterministic component and a set of lags of the dependent variable to account for potential autocorrelation, yields the following specific HEGY test regression for unit roots in monthly data ( $S = 12$ )

$$\begin{aligned} \Delta_{12}y_{12n+s} &= \mu_{S_{n+s}} + \pi_0 z_{0,12n+s-1} + \pi_6 z_{6,12n+s-1} \\ &\quad + \sum_{k=1}^5 (\pi_{\alpha k} z_{k,12n+s-1}^\alpha + \pi_{\beta k} z_{k,12n+s-1}^\beta) + \sum_{l=1}^p \phi_l \Delta_{12}y_{12n+s-l} + \varepsilon_{12n+s} \end{aligned} \quad (3.1)$$

where the regressor variables in (3.1) used to test for the unit roots are linear transformations of lagged values of  $y_{S_{n+s}}$ ,  $\mu_{S_{n+s}}$  represents a deterministic kernel (a set of seasonal dummies or a set of seasonal dummies and trend) and  $p$  is the order of lag augmentation considered. The regressors used to test for the zero and Nyquist frequencies unit roots are given as

$$z_{0,12n+s} = \sum_{j=0}^{11} L^j y_{12n+s}, \quad z_{6,12n+s} = \sum_{j=0}^{11} \cos[(j+1)\pi] L^j y_{12n+s}$$

while the pairs of variables that test the complex unit roots at other frequencies are

$$z_{k,12n+s}^\alpha = \sum_{j=0}^{11} \cos[(j+1)\omega_k] L^j y_{12n+s}; \quad \text{and} \quad z_{k,12n+s}^\beta = - \sum_{j=0}^{11} \sin[(j+1)\omega_k] L^j y_{12n+s}$$

where  $\omega_k = 2\pi k/12$ ,  $k = 1, \dots, 5$ . The variables just defined have the effect of imposing all unit roots implied by  $\Delta_{12}$  except for a single unit root (or, for the pair  $z_{k,12n+s}^\alpha$  and  $z_{k,12n+s}^\beta$ , a pair of complex unit roots) and hence the respective coefficient(s) evaluate the nonstationary dynamic properties of the process at a specific frequency.

More specifically, the presence of unit roots implies exclusion restrictions for the coefficients  $\pi_0$ ,  $\pi_6$  and the pairs  $\pi_{\alpha k}$ ,  $\pi_{\beta k}$ ,  $k = 1, \dots, 5$ ; the overall null hypothesis of seasonal integration implies all these are zero. To test seasonal integration against stationarity at one or more of the seasonal or nonseasonal frequencies, HEGY suggest using:  $t_0$  (left-sided) for the exclusion of  $z_{0,12n+s}$ ;  $t_6$  (left-sided) for the exclusion of  $z_{6,12n+s-1}$ ;  $F_k$  for the exclusion

of both  $z_{k,12n+s-1}^\alpha$  and  $z_{k,12n+s-1}^\beta$ ,  $k = 1, \dots, 5$ . These tests examine the potential unit roots separately at each of the zero and seasonal frequencies, raising issues of the significance level for the overall test (Dickey, 1993). Consequently, Ghysels, Lee and Noh (1994) also consider joint frequency OLS  $F$ -statistics. Specifically  $F_{1\dots 6}$  tests for the presence of all seasonal unit roots by testing for the exclusion of  $z_{6,12n+s-1}$  and  $\{z_{k,12n+s-1}^\alpha, z_{k,12n+s-1}^\beta\}_{k=1}^5$ , while  $F_{0\dots 6}$  examines the overall null hypothesis of seasonal integration, by testing for the exclusion of all regressors in (3.1). These joint tests are further considered by Taylor (1998) and Smith and Taylor (1998, 1999).

In Table 3.2 we present the results for the test statistics just described obtained from the application of the test regression of the form of (3.1), augmented with a set of seasonal dummies and lags of the dependent variable, on the IPI series. The maximum lag order considered for augmentation was 24 and a testing down procedure, as suggested by Ng and Perron (1995), used to determine the effective lag order (this order is indicated in Table 3.2 in the column Augment). The test regression was also applied with a set of seasonal dummies and a time trend, however the results were qualitatively similar (see Table A.1 in the appendix).

**Table 3.2: Testing for Seasonal Unit Roots in Industrial Production Series**

| Country     | $t_0$ | $t_6$  | $F_1$  | $F_2$  | $F_3$  | $F_4$  | $F_5$  | $F_{1\dots 6}$ | $F_{0\dots 6}$ | Augment |
|-------------|-------|--------|--------|--------|--------|--------|--------|----------------|----------------|---------|
| Austria     | 0.71  | -1.38  | 2.03   | 7.14*  | 6.11   | 8.04*  | 2.64   | 5.57*          | 5.17*          | 19      |
| Canada      | -0.84 | -1.32  | 5.08   | 3.03   | 12.29* | 4.79   | 4.14   | 6.54*          | 6.07*          | 24      |
| Denmark     | -1.64 | -1.09  | 4.26   | 4.35   | 3.62   | 7.72*  | 7.62*  | 5.43*          | 5.22*          | 24      |
| Finland     | -0.74 | -1.17  | 0.92   | 0.39   | 5.78   | 0.46   | 1.40   | 1.78           | 1.70           | 21      |
| France      | -0.38 | -3.31* | 5.28   | 8.77*  | 4.96   | 7.46*  | 2.80   | 7.98*          | 6.60*          | 18      |
| Germany     | -1.59 | -0.68  | 2.19   | 8.79*  | 4.53   | 5.06   | 1.38   | 4.34           | 4.23           | 24      |
| Greece      | 0.12  | -2.23  | 6.25   | 5.90   | 2.89   | 4.21   | 0.85   | 4.38           | 4.02           | 24      |
| Hungary     | -1.08 | -0.81  | 6.59   | 2.78   | 3.75   | 9.74*  | 2.44   | 5.19*          | 4.86           | 17      |
| Italy       | -1.67 | -2.22  | 1.30   | 5.49   | 2.31   | 2.04   | 2.46   | 3.15           | 3.14           | 24      |
| Japan       | -2.51 | -1.19  | 5.13   | 5.56   | 1.71   | 4.16   | 6.30   | 4.66           | 4.94           | 23      |
| Luxembourg  | -0.79 | -2.28  | 14.96* | 4.73   | 4.82   | 3.09   | 6.88   | 7.75*          | 7.17*          | 20      |
| Netherlands | -0.07 | -1.82  | 8.71*  | 6.65   | 6.71   | 5.06   | 1.83   | 6.04*          | 5.54*          | 12      |
| Portugal    | -1.35 | -1.68  | 2.66   | 3.11   | 0.43   | 0.84   | 2.74   | 2.12           | 2.15           | 24      |
| Spain       | -0.78 | -1.16  | 1.46   | 2.12   | 1.77   | 1.44   | 0.78   | 1.54           | 1.48           | 15      |
| Sweden      | 0.24  | -1.14  | 1.49   | 1.18   | 1.84   | 0.90   | 1.07   | 1.35           | 1.24           | 21      |
| UK          | -1.42 | -2.96* | 4.57   | 17.47* | 7.74*  | 8.60*  | 1.37   | 9.59*          | 9.09*          | 20      |
| USA         | 0.08  | -2.50  | 11.94* | 7.14*  | 12.76* | 10.46* | 17.48* | 13.14*         | 12.05*         | 4       |
| Euro Area   | -1.03 | -1.28  | 2.49   | 6.61   | 3.00   | 5.84   | 1.11   | 3.75           | 3.56           | 17      |

Note: \* denotes significance at the 5% nominal level. The critical values considered were computed from a HEGY test regression such as (3.1) augmented with a set of seasonal dummies and a set of lags of the dependent variable (the maximum lag order considered for all cases was 24 lags), the data was generated from a monthly seasonal random walk and 50000 Monte Carlo replications used.  $t_0$  and  $t_6$ , represent the one sided unit root t-test statistics at frequencies 0 and  $\pi$ , respectively;  $F_1, F_2, F_3, F_4$  and  $F_5$ , correspond to the joint tests for seasonal unit roots at frequencies  $(\frac{\pi}{2}, \frac{3\pi}{2})$ ,  $(\frac{5\pi}{3}, \frac{7\pi}{6})$ ,  $(\frac{\pi}{6}, \frac{11\pi}{6})$ ,  $(\frac{2\pi}{3}, \frac{4\pi}{3})$  and  $(\frac{\pi}{3}, \frac{5\pi}{6})$ , respectively; and  $F_{1\dots 6}$  and  $F_{0\dots 6}$

represent the joint tests for unit roots at all seasonal frequencies and at all frequencies, respectively. The column order identifies the order of the lag length considered in each test regression. The critical values considered were: -2.80 for the zero and Nyquist frequency unit roots; 5.04 and 4.98 for the  $F_{1\dots 6}$  and  $F_{0\dots 6}$  tests, respectively and 7.09 for the  $F_i$ ,  $i = 1, \dots, 5$ , tests.

The overall test statistics  $F_{1\dots 6}$  and  $F_{0\dots 6}$  of Table 3.2 reject the presence of the full set of seasonal unit roots for about half of the series. However, for a group of European countries (namely, Finland, Greece, Italy, Portugal and Spain, as well as the Euro area as a whole) the data does not reject the unit root at any frequency, providing relatively strong support in favour of seasonal integration. The strongest evidence against the presence of seasonal unit roots occurs for the UK and USA.

### 3.3. Nonlinearity

As an indicator of the potential value of SETAR models for our seasonal series, we test for the presence of threshold effects in the data by investigating whether the difference between the coefficients in the regimes is significant in (2.7).

Order selection for the autoregressive component of the seasonal SETAR model is also important. In this study, the order of the test regressions employed was determined following a general-to-specific procedure (see Ng and Perron, 1995) in a linear AR model, using a maximum lag of  $p = 12$ . The p-values for the linearity test are obtained using the bootstrap, as suggested by Hansen (1997) in this context. Our application uses 5000 bootstrap replications.

Table 3.3 presents the results of tests of linearity against SETAR type nonlinearity of the industrial production series. These results are obtained from a regression of the form of (2.7) where  $q_{12n+s-d} = \Delta_{12}y_{12n+s-d}$  and the delay  $d$  and the threshold value  $\gamma$  are endogenously determined from a search over the central 70% of the empirical distribution of  $\Delta_{12}y_{12n+s-d}$ . The maximum delay considered for determining  $d$  was the effective order of the regression considered (as given in the column *AR order* in Table 3.3).

From Table 3.3, we observe that the linear structure is rejected for around half of the countries considered, with the strongest evidence of nonlinearity being for Germany, Sweden and the Euro Area.

**Table 3.3: Testing for Linearity in Industrial Production Series**

| Country     | $\gamma$ | $d$ | Linearity test (p-value) | AR order |
|-------------|----------|-----|--------------------------|----------|
| Austria     | -.005    | 4   | .016                     | 12       |
| Canada      | -.015    | 1   | .121                     | 10       |
| Denmark     | .052     | 4   | .052                     | 12       |
| Finland     | .030     | 12  | .218                     | 12       |
| France      | .019     | 8   | .167                     | 12       |
| Germany     | .037     | 5   | .007                     | 12       |
| Greece      | .027     | 5   | .037                     | 12       |
| Hungary     | .117     | 9   | .023                     | 12       |
| Italy       | .078     | 12  | .112                     | 12       |
| Japan       | -.026    | 2   | .054                     | 10       |
| Luxembourg  | .094     | 8   | .024                     | 12       |
| Netherlands | -.065    | 6   | .029                     | 12       |
| Portugal    | -.003    | 7   | .070                     | 12       |
| Spain       | .014     | 6   | .464                     | 12       |
| Sweden      | .021     | 9   | .001                     | 12       |
| UK          | .045     | 1   | .129                     | 10       |
| USA         | -.051    | 2   | .067                     | 9        |
| Euro Area   | .014     | 10  | .001                     | 12       |

### 3.4. Periodicity

Given that monthly data are used in this paper, an obvious PAR model to consider is a  $PAR(12, p)$ , which identifies each month as a distinct "season". However, if used without restrictions, this model has the potential disadvantage of being highly parameterised. For instance, an unrestricted  $PAR(12, 12)$ , even with no deterministic terms, requires estimation of  $12 \times 12 = 144$  coefficients. Hence, this raises interest in identifying more parsimonious models.

One strategy adopted below is based on the assumption that common behaviour is present for specific months, leading to the proposal of a  $PAR(3, p)$  model. These  $PAR(3, p)$  models are determined based on the classification of the monthly data into three distinct groups of months, with one group including all months with negative average monthly growth, another all months with relatively low monthly positive growth and the third group includes months with the strongest observed average monthly growth<sup>1</sup>. This grouping leads to three "seasons" with different numbers of observations.

In a similar way as for non-linearity, we also test the presence of periodic coefficient variation, to examine whether the data display this characteristic. The results are in Table 3.4.

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<sup>1</sup>To be specific, the positive growth regime classifications generally used an average growth of less than 0.1% per month as low growth and monthly growth of 0.1% or more as high growth. However, different classification rules were used for the Canada and the US, for which low (positive) growth was defined in relation to thresholds of 0.03% and 0.05%, respectively.

### [Insert Table 3.4 about here]

The test procedures denoted as  $F_{PeAR1\_12}$  and  $F_{SH}$  are applied to the residuals of an AR model as described in (2.11) and (2.12) fitted to the annually differenced series. The  $F_{PAR(.)}$  test is applied to the levels of the data. The maximum lag length of the AR considered is 12 in both cases, which was reduced where appropriate based on a testing down strategy.

Whether applied to the residuals or the levels of the data, Table 3.4 provides strong evidence in favour of the presence of periodic coefficient variation across the IPI series analysed. When directly applied to the coefficients, however, the  $F_{PAR(3)}$  test rejects substantially less than does  $F_{PAR(12)}$ . Note, however, that the regression on which the latter test is based is highly parameterised, so the results may not be entirely reliable. The  $F_{SH}$  test provides only weak evidence of seasonal heterocedasticity across the series considered. Nevertheless, the other results point to the potential value of using periodic models for forecasting.

## 4. Forecast Accuracy

To evaluate forecast accuracy, consider the use of  $m$  post-sample observations to evaluate  $h$ -step ahead forecasts generated from models fitted to the first  $T$  observations.

Although many measures of forecast accuracy are available, we follow much of the literature in basing our evaluation on the Root Mean Squared Prediction Error ( $RMSPE$ ), defined as

$$RMSPE(h) = \sqrt{\frac{1}{m-h+1} \sum_{j=h}^{T+m} (\hat{y}_{T+j|T+j-h} - y_{T+j})^2} \quad (4.1)$$

where  $\hat{y}_{T+j|T+j-h}$  is the  $h$ -step ahead forecast made for period  $T+j$  based on data available at  $T+j-h$ . In order to focus on the role of seasonality, which may be anticipated to be most marked for short-term forecasts of less than a year, results are computed for horizons  $h = 1, 3, 8$ .

In this paper, nonlinear time series models are compared with linear and periodic models. To reflect the different approaches to treating seasonality in linear models, we consider specifications based on various levels of differencing, namely no differences, together with models after application of the filters  $\Delta_{12}, \Delta_1$  and  $\Delta_{12}\Delta_1$ . All forecasts are considered in relation to the level of the IPI series using RMSPE as defined in (4.1).

There is growing empirical evidence that nonlinear models perform relatively well for long term forecasting and that linear models dominate in the short run (see, *inter alia*, Terui and van Dijk, 1999). Clements *et al.* (2003) compare linear autoregressive and SETAR models and study the degree of non-linearity that needs to be present in the data before forecasts from non-linear models outperform linear rivals. For interesting overviews on comparing forecast accuracy see, *inter alia*, Franses and van Dijk (2000) and Diebold and Mariano (1995).

### 4.1. Nonlinear Model Forecasts

The nonlinear (seasonal) SETAR models we employ are based on (2.7). For such models, computing point forecasts is considerably more involved than computing forecasts from linear

models. To illustrate this, consider the case where the variable  $y_{S_n+s}$  is described by a first order nonlinear autoregressive model which is summarised as,

$$y_{S_n+s} = F(y_{S_n+s-1}; \theta) + \varepsilon_{S_n+s}. \quad (4.2)$$

In this context, when the forecast horizon is longer than 1 period, the linear conditional expectation operator can not be interchanged with the nonlinear operator  $F$ , since

$$E[F(\cdot)] \neq F(E[\cdot]).$$

Since the expected value of a nonlinear function is not equal to the function evaluated at the expected value of its argument, then for a given parameter vector  $\theta$  and horizon  $h$

$$E[F(y_{S_n+s+h-1}; \theta) | \Omega_{S_n+s}] \neq F(E[(y_{S_n+s+h-1|S_n+s}) | \Omega_{S_n+s}]; \theta), \quad h > 1$$

where  $\Omega_{S_n+s}$  indicates information available at time  $S_n + s$ . However, an unbiased point forecast based on (4.2) requires estimation of the left-hand side of this expression.

The distribution of the white noise disturbance  $\varepsilon_{S_n+s}$  in (4.2) is never known with certainty. However, to overcome this difficulty, forecasts can be computed using Monte Carlo or Bootstrap methods. Lin and Granger (1994) and Clements and Smith (1997) compare various methods to obtain multiple-step-ahead forecasts for SETAR models and conclude that the bootstrap method compares favourably to the other methods. This is the method also adopted in this paper, where we use 500 bootstrap replications in order to approximate  $E[F(y_{S_n+s+h-1}; \theta) | \Omega_{S_n+s}]$ . For interesting reviews see, *inter alia*, Franses and Van Dijk (2001, pp. 119-121), Lin and Granger (1994) and Clements and Smith (1997).

## 4.2. Methods for Forecast Combinations

Combining forecasts, as introduced by Bates and Granger (1969), has often been found to improve forecast accuracy compared with using an individual forecasting method. The effectiveness of simple averaging is demonstrated by, among others, Bates and Granger (1969), Granger and Newbold (1977) and Granger and Ramanathan (1984), while other articles demonstrate the usefulness of other approaches to combining multiple individual forecasts; see, *inter alia*, Armstrong (1989, 2001); Clemen (1989), Diebold and Lopez (1996), Hendry and Clements (2002), Markridakis and Winkler (1983); Markridakis *et al.* (1982), Newbold and Harvey (2002), Stock and Watson (1999), Terui and van Dijk (2002).

The remainder of this section briefly introduces the forecast combination methods that we employ in our empirical analysis. In addition to simple averages (mean or median), methods for combining forecasts can be classified as being based on historical RMSPE or derived from regression methods. We devote separate subsections to each of these approaches.

## 4.3. Historical RMSPE Forecasts

The historical RMSPE forecasts consider the forecast combination as a weighted average of the individual forecasts, with the weights varying with the historical performance of each individual forecast; see, *inter alia*, Diebold and Pauly (1987) and Stock and Watson (1999).

For  $k$  separate  $h$ -step forecasts, namely  $\hat{y}_{S_{n+s+h}|S_{n+s}}^i$  ( $i = 1, \dots, k$ ), the forecast combination is given by

$$\hat{y}_{S_{n+s+h}|S_{n+s}}^c = \sum_{i=1}^k w_i^h \hat{y}_{S_{n+s+h}|S_{n+s}}^i$$

where the weight  $w_i^h$  is

$$w_i^h = [1/RMSPE(h)_i]^\lambda / \sum_{j=1}^k [1/RMSPE(h)_i]^\lambda \quad (4.3)$$

and  $RMSPE(h)_i$  the Root Mean Square Predictor Error for method  $i$  at horizon  $h$ . Since the relative performance of different models can change over time, following Bates and Granger (1969) we compute RMSPE at the end of the sample  $T$  using information relating to forecasts for the final three years of the estimation sample, namely  $T - 35$  to  $T$ .

As implied by (4.3), the weights on the constituent forecasts are inversely related to their RMSPE values (note that the weights are initially based on RMSPE calculated using within-sample observations). A simple average which places equal weight on all forecasts corresponds to  $\lambda = 0$ . As  $\lambda$  increases, a weight is placed on those models that have been performing relatively well. In this paper we consider  $\lambda \in \{0, 1, 1.25, 1.5, 2\}$ , with  $\lambda = 2$  implying that the weights are inversely proportional to the mean square prediction error.

In addition to weighting as in (4.3), we consider also weights that discount historical forecast accuracy based on RMSPE (see Stock and Watson, 2003). For an  $h$ -step forecast, the combination weight in this case has the form

$$w_i^h = (m_i^h)^{-1} / \sum_{j=1}^k (m_j^h)^{-1} \quad (4.4)$$

where

$$m_i^h = \sqrt{\sum_{j=1}^{T-h} \delta^{j-1} (\hat{y}_{T-j+1|T-j+1-h}^i - y_{T-j+1})^2} \quad (4.5)$$

and  $\delta$  is the discount factor. In this paper, we consider three values for the discount factor  $\delta \in \{1, 0.95, 0.90\}$ . Note that for  $\delta = 1$  (4.5) operates as a window with no discounting and this weighting scheme is then equivalent to (4.3) with  $\lambda = 2$  when the latter uses all observations to time  $T$ .

#### 4.4. Regression Methods

Granger and Ramanathan (1984), Diebold (1988) and others, suggest combining forecasts using regression methods. Following Diebold (1988), we consider a framework where relaxation of the zero constant and the weights summing to unity is allowed. Following Diebold (2001, p.297) it is preferable not to force the weights to add to unity, or to exclude an intercept. Indeed, inclusion of an intercept facilitates bias correction and allows biased forecasts

to be combined. Therefore, the regression used can be expressed as

$$y_{S_n+s+h} = \beta_0 + \sum_{j=1}^k \beta_j \hat{y}_{S_n+s+h|S_n+s}^j + \varepsilon_{S_n+s+h} \quad (4.6)$$

with  $j = 1, 2, \dots, k$ , and where  $k$  represents the number of individual forecast methods. The weights in (4.6) for the observation at  $T$  are estimated using the final 36 observations in the estimation period, namely corresponding to  $h$ -step ahead forecasts for periods  $T - 35$  to  $T$  inclusive.

However, with  $k = 17$  in our case, (4.6) implies an excessive parameterisation. Therefore, in implementing (4.6) we use only the five methods producing the most accurate forecasts over the latest available 36 observations.

## 5. Forecast Performance

### 5.1. Methods Employed

Table 5.1 presents the individual forecasting models that we apply, while the 18 forecast combination procedures used are summarised in Table 5.2.

As evident from Table 5.1, the models of Section 2 are generally applied to data after differencing. Since the appropriate level of differencing is often unclear in empirical analyses, we reflect this uncertainty by applying the same models to data differenced to different levels. For example, low-order ARMA models are applied to data after annual differencing, and to data after both first and annual differences are applied; PAR and SETAR models are estimated for levels and first differenced data. In each case these choices reflect the type of data to which these models are applied in practice, in conjunction with the indicated deterministic terms. For the  $AR(p)$  models of Table 5.1, a maximum order of 24 is considered, while the  $SETAR(p_1, p_2)$  considers a maximum order of 12. In both cases, insignificant lags are eliminated (starting with the minimum  $t$ -statistic) prior to using the models for forecasting.

**Table 5.1 - Forecast Models**

| Code | Individual Models    | Filter                | Deterministic terms                   |
|------|----------------------|-----------------------|---------------------------------------|
| M1   | <i>Airline Model</i> | $\Delta_1\Delta_{12}$ | None                                  |
| M2   | $ARMA(1, 1)$         | $\Delta_{12}$         | Intercept                             |
| M3   | $ARMA(2, 2)$         | $\Delta_{12}$         | Intercept                             |
| M4   | $AR(p)$              | $\Delta_{12}$         | Intercept                             |
| M5   | $SSETAR(p_1, p_2)$   | $\Delta_{12}$         | Intercept                             |
| M6   | $AR(p)$              | <i>levels</i>         | Seasonal intercepts + trend           |
| M7   | $PAR(12, 3)$         | <i>levels</i>         | Seasonal intercepts + trend           |
| M8   | $PAR(3, 3)$          | <i>levels</i>         | Seasonal intercepts & seasonal trends |
| M9   | $SSETAR(p_1, p_2)$   | <i>levels</i>         | Seasonal intercepts & seasonal trends |
| M10  | $AR(p)$              | $\Delta_1$            | Seasonal intercepts                   |
| M11  | $PAR(3, 3)$          | $\Delta_1$            | Seasonal intercepts + trend           |
| M12  | $PAR(12, 3)$         | $\Delta_1$            | Seasonal intercepts & seasonal trends |
| M13  | $SSETAR(p_1, p_2)$   | $\Delta_1$            | Seasonal intercepts                   |
| M14  | $ARMA(1, 1)$         | $\Delta_1\Delta_{12}$ | None                                  |
| M15  | $ARMA(2, 2)$         | $\Delta_1\Delta_{12}$ | None                                  |
| M16  | $ARMA(3, 3)$         | $\Delta_1\Delta_{12}$ | None                                  |
| M17  | $AR(p)$              | $\Delta_1\Delta_{12}$ | None                                  |

The combination methods that we consider are based *i*) on the weight function, (4.3) with  $S = 12$  and  $\lambda \in (0, 1, 1.25, 1.5, 2)$ ; *ii*) on the mean and median of the best 5, 10 and 15 models which are chosen based on the historical RMSPE across the 17 models considered; *iii*) on the discounted RMSPE weights as given in (4.4) and (4.5) with  $S = 12$  and  $\delta \in \{1, 0.95, 0.90\}$ ; *iv*) based on the regression method as described in (4.6); *v*) and finally, on the mean or median of all combinations. Table 5.2 summarizes the individual combination methods used in the empirical analysis.

**Table 5.2 - Combination Methods**

| Code | Combination method                        | parameters       |
|------|---|------------------|
| C1   | mean of M1 to M17                         |                  |
| C2   | median of M1 to M17                       |                  |
| C3   | (4.3)                                     | $\lambda = 0$    |
| C4   | (4.3)                                     | $\lambda = 1$    |
| C5   | (4.3)                                     | $\lambda = 1.25$ |
| C6   | (4.3)                                     | $\lambda = 1.5$  |
| C7   | (4.3)                                     | $\lambda = 2$    |
| C8   | mean of best 5 models (RMSPE criteria)    |                  |
| C9   | mean of best 10 models (RMSPE criteria)   |                  |
| C10  | mean of best 15 models (RMSPE criteria)   |                  |
| C11  | median of best 5 models (RMSPE criteria)  |                  |
| C12  | median of best 10 models (RMSPE criteria) |                  |
| C13  | median of best 15 models (RMSPE criteria) |                  |
| C14  | mean of combinations                      |                  |
| C15  | (4.4) and (4.5)                           | $\delta = 1$     |
| C16  | (4.4) and (4.5)                           | $\delta = 0.95$  |
| C17  | (4.4) and (4.5)                           | $\delta = 0.9$   |
| C18  | regression method of (4.6)                |                  |

## 5.2. Forecasting Results

Forecast accuracy is evaluated by employing the final 36 observations (January 2003 to December 2005, inclusive) to provide post-sample actual values. All forecasting models are recursively re-estimated over this forecasting period. In addition, models that require specification of the appropriate AR order are also recursively re-specified during the forecast period, while the weights required in (4.3), (4.4) and (4.6) are also updated using the most recently available observations and the corresponding forecast values.

Tables 5.3a to 5.3e contain the individual results for each of the countries considered (including the Euro Area). Not surprisingly, the best performing methods differ over both the horizon ( $h = 1, 3, 8, 12$ ) considered and the country. However, two cases of particular interest might be the US and Euro Area. For the former, the simple  $AR(p)$  model M6 estimated in levels does well at short horizons ( $h = 1, 3$ ), but this model is relatively poor at longer horizons. On the other hand, the  $PAR(3,3)$  model M11 in first differences is the most accurate method at a horizon of  $h = 8$  months and provides relatively good performance at  $h = 3, 12$  but not at one month ahead. These last results are compatible with the evidence against the seasonal integration for this series in Table 3.2 and that in favour of the periodic model in Table 3.4. Nevertheless, the best overall results for the US are given by combining forecasts using the median forecast from the most accurate 5 models. This combination yields the most accurate US forecasts at horizons of one and 12 months, a close competitor to the best at  $h = 3$  and the fifth most accurate at  $h = 8$ .

For the Euro Area, a good performance of the  $PAR(3,3)$  model M11 at  $h = 1, 3$  and 8 is observed, although this does not carry over to the longer horizon of  $h = 12$  where seasonality is not expected to play a strong role. The closest competitor at very short horizons is another PAR model in levels, namely M12. For the Euro Area, however, it is striking that combinations perform well at  $h = 8$ , and a variety of combined forecasts are more accurate than any individual model at  $h = 12$ . In common with the US, the median of the best 5 forecasts is the most accurate of all considered at the one year horizon.

Across all the sub-tables in Table 5.3 it is easier to pick out consistently poor forecasting models than consistently good ones. Indeed, the SETAR models M9 and M13 are frequently the worst performing individual models. This may be a consequence of the nonlinearity often evident in Table 3.3 not being repeated during the forecast period.

**[Insert Tables 5.3a to 5.3e about here]**

From the detailed results of Tables 5.3a to 5.3e, we observe that the top five forecasting models across all countries considered can be classified as follows: for  $h = 1$ , combinations occupy 72% of the top five positions compared with only 28% from the individual models; for  $h = 3$ , forecast combinations take 57% of the top five positions; for  $h = 8$ , the distribution becomes slightly more symmetric in that combinations represent 54% of the top five positions and finally for  $h = 12$  combinations account for only 44% of the top five positions. In this sense, the result for the US and the Euro Area that combinations do best at this one year horizon is not typical of all countries considered.

Table 5.4 allows general comparisons across rankings and RMSPE. Note that in Table 5.4 results for the RMSPE of the models and combinations considered are scaled by that of M1 at each horizon in order to facilitate comparisons. Here some individual linear models perform reasonably well, including the Airline model (M1) and the PAR models M7, M8, M11 and M12 as well as the *SARIMA* model M17. It should be noted that the Airline and the *AR* models, M1 and M17 take account of seasonality only in the naive fashion of largely removing it through the application of annual (in addition to first) differences. Although a number of individual models provide more accurate forecasts than the Airline model in terms of average relative RMSPE at  $h = 1$ , the robust performance of this model becomes notable at longer horizons in Table 5.4, with no individual model providing more accurate average relative RMSPE at either  $h = 8$  or 12.

**[Insert Table 5.4 about here]**

The poor performance of the *SETAR* model in levels (M9) and first differences (M13) is particularly marked in Table 5.4. These results are also not favourable overall to the use of *ARMA* specifications after first and annual differences (M14, M15, M16) for forecasting these IPI series. Thus, at least for this period, these are not favoured for forecasting seasonal IPI at short horizons.

The average rankings in Table 5.4 are, however, quite explicit as to the quality of the forecast combinations, with the overall average rankings for the forecast combinations being in general superior to the forecast models considered. Indeed, in terms of rankings, combinations always occupy the top places.

For  $h = 1$ , the best average performance is given by the combinations C17 (discounted RMSPE forecast weights based on (4.4) and (4.5) with  $\delta = 0.90$ ), followed by C4, C15, C16.. For  $h = 3$  the best overall average performance is C15 (undiscounted RMSPE forecasts based on (4.4) and (4.5) with  $\delta = 1$ ) and C4 and C5. For  $h = 8$ , the best performance is C16 (discounted RMSPE forecasts based on (4.4) and (4.5) with  $\delta = 0.95$ ), followed by C4, C10 and C17. Finally, for  $h = 12$ , the best average ranking is observed for C8 (mean of best 5 models) followed by C17, C6, C7 and C16. Overall, therefore, rankings point to the use of forecast combination methods that use previous RMSPE performance as weights.

Table 5.4 also indicates that almost all combination methods considered give average RMSPE gains compared to even the best of the individual models for the short horizons  $h = 1, 3$ . The only exceptions to this are C1 (mean of all models) and C3 ((4.3) with  $\lambda = 0$ ) and C18 (regression method of (4.6)).

## 6. Conclusion

This study reinforces evidence that combining forecasts from individual models improves post-sample forecast accuracy. Our conclusion is based on forecasts from a large set of individual models and methods of combination of forecasts, whose performance is evaluated using monthly seasonally unadjusted Industrial Production data from 17 individual countries (Austria, Canada, Denmark, Finland, France, Germany, Greece, Hungary, Italy, Japan, Luxembourg, Netherlands, Portugal, Spain, Sweden, United Kingdom and USA) and an aggregate series for the Euro Area.

The potential of forecast combinations is even more attractive in the context of seasonal data than data after seasonal adjustment, due to the number of questions that arise in the analysis of seasonal data. For instance, there are questions as to the stationarity or otherwise of seasonal dynamics, whether capturing seasonality requires the use of periodic (seasonally-varying coefficient) models and whether there are nonlinear seasonal/business cycle interactions. According to our results, almost all forecast combination methods deliver improved forecast performance over individual methods. Nevertheless, the combination methods that produce the most accurate forecasts in our study identify the best forecasting models and base the combination on these. Indeed, a simple average of the best five forecasting models for a particular horizon is a robust method that reasonably performs well, especially when forecasting one month ahead. Nevertheless, we find that better combinations can usually be found by weighting the forecasts using information from the root mean-square prediction error for earlier periods.

Our results relating to the use of more complex methods of handling seasonality are mixed, in the sense that nonlinear models here deliver poor forecast performance, whereas a parsimonious parameterisation of a periodic model performs relatively well at very short horizons of one and three months. However, relatively high parameterisations are typically implied by these complex methods, and future research may examine further the extent to which the imposition of restrictions can improve this performance.

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## Appendix

**Table A.1. - Testing for Seasonal Unit Roots in Industrial Production Series**  
 (Results from HEGY Test Regression with Seasonal Dummies and Time Trend)

| Country     | $t_0$ | $t_6$  | $F_1$  | $F_2$  | $F_3$  | $F_4$ | $F_5$ | $F_{1\dots 6}$ | $F_{0\dots 6}$ | Augment'n |
|-------------|-------|--------|--------|--------|--------|-------|-------|----------------|----------------|-----------|
| Austria     | -1.92 | -1.37  | 1.98   | 7.07   | 6.23   | 7.94* | 2.47  | 5.51*          | 5.50*          | 19        |
| Canada      | -1.89 | -1.33  | 5.15   | 3.03   | 12.47* | 4.81  | 4.03  | 6.59*          | 6.40*          | 24        |
| Denmark     | -2.72 | -1.10  | 4.42   | 4.31   | 3.82   | 7.96* | 8.27* | 5.65*          | 5.79*          | 24        |
| Finland     | -2.81 | -0.99  | 0.74   | 0.15   | 4.87   | 0.34  | 1.47  | 1.48           | 2.12           | 18        |
| France      | -2.89 | -3.34* | 5.20   | 8.82*  | 5.31   | 7.25* | 3.03  | 7.29*          | 7.57*          | 18        |
| Germany     | -1.73 | -0.69  | 2.25   | 8.85*  | 4.61   | 5.10  | 1.41  | 4.39           | 4.28           | 24        |
| Greece      | -1.19 | -2.23  | 6.25   | 5.94   | 2.87   | 4.21  | 0.84  | 4.37           | 4.12           | 24        |
| Hungary     | -1.72 | -0.81  | 6.57   | 2.72   | 3.76   | 9.80* | 2.42  | 5.19*          | 5.05           | 17        |
| Italy       | -1.96 | -2.45  | 1.78   | 7.22*  | 2.78   | 2.08  | 2.57  | 3.85           | 3.92           | 18        |
| Japan       | -2.33 | -1.18  | 5.08   | 5.50   | 1.70   | 4.08  | 6.55  | 4.67           | 4.52           | 23        |
| Luxembourg  | -2.65 | -2.31  | 14.90* | 4.64   | 4.90   | 3.01  | 6.69  | 7.69*          | 7.95*          | 20        |
| Netherlands | -2.90 | -1.85  | 8.87*  | 6.76   | 6.96   | 5.11  | 1.75  | 6.15*          | 6.46*          | 12        |
| Portugal    | -1.54 | -1.68  | 2.76   | 3.10   | 0.41   | 0.84  | 2.81  | 2.15           | 2.18           | 24        |
| Spain       | -2.54 | -1.15  | 1.44   | 2.21   | 1.56   | 1.45  | 1.01  | 1.56           | 2.05           | 15        |
| Sweden      | -2.54 | -1.12  | 1.56   | 1.26   | 1.77   | 0.86  | 1.16  | 1.36           | 1.87           | 21        |
| UK          | -1.75 | -2.99* | 4.54   | 17.20* | 7.69*  | 8.49* | 1.28  | 9.50*          | 9.18*          | 20        |
| USA         | -2.61 | -1.19  | 10.75* | 3.99   | 5.45   | 6.45  | 7.84* | 7.06*          | 7.29*          | 17        |
| Euro Area   | -2.96 | -1.12  | 2.89   | 7.03   | 3.46   | 6.47  | 0.79  | 4.01           | 4.71           | 16        |

**Note:** \* denotes significance at the 5% nominal level. The critical values considered were computed from a HEGY test regression such as (3.1) augmented with a set of seasonal dummies and a time trend, and a set of lags of the dependent variable (the maximum lag order considered for all cases was 24 lags) and the data was generated from a monthly seasonal random walk.  $t_0$  and  $t_6$ , represent the one sided unit root t-test statistics at frequencies 0 and  $\pi$ , respectively;  $F_1, F_2, F_3, F_4$  and  $F_5$ , correspond to the joint tests for seasonal unit roots at frequencies  $(\frac{\pi}{2}, \frac{3\pi}{2})$ ,  $(\frac{5\pi}{3}, \frac{7\pi}{6})$ ,  $(\frac{\pi}{6}, \frac{11\pi}{6})$ ,  $(\frac{2\pi}{3}, \frac{4\pi}{3})$  and  $(\frac{\pi}{3}, \frac{5\pi}{6})$ , respectively; and  $F_{1\dots 6}$  and  $F_{0\dots 6}$  represent the joint tests for unit roots at all seasonal frequencies and at all frequencies, respectively. The column order identifies the order of the lag length considered in each test regression. The critical values considered were: -3.38 for the zero frequency, -2.80 for the Nyquist frequency; 5.03 and 5.27 for the  $F_{1\dots 6}$  and  $F_{0\dots 6}$  tests, respectively and 7.08 for the  $F_i$ ,  $i = 1, \dots, 5$ , tests.

**Table 3.4: Testing for Periodicity**

|             | $F_{PeARI_{-12}}$    |                       |                      | $F_{SH}$             |                       |                      |
|-------------|----------------------|-----------------------|----------------------|----------------------|-----------------------|----------------------|
|             | PAR(3) <sup>a)</sup> | PAR(12) <sup>b)</sup> | PAR(3) <sup>a)</sup> | PAR(3) <sup>a)</sup> | PAR(12) <sup>b)</sup> | PAR(3) <sup>a)</sup> |
| Austria     | 1.83* (36,191)       | 1.37* (144,83)        | 3.69* (2,227)        | 3.50* (11,227)       | 2.05* (24,235)        | 1.52* (132,118)      |
| Canada      | 2.73* (36,195)       | 1.55* (144,87)        | 0.08 (2,231)         | 1.50 (11,231)        | 8.24* (8,259)         | 3.07* (44,214)       |
| Denmark     | 3.35* (36,191)       | 2.79* (144,83)        | 3.14* (2,227)        | 1.66 (11,227)        | 0.64 (24,235)         | 1.92* (132,118)      |
| Finland     | 1.59* (36,191)       | 1.66* (144,83)        | 3.08* (2,227)        | 1.79 (11,227)        | 1.14 (24,235)         | 4.51* (132,118)      |
| France      | 1.85* (36,191)       | 2.00* (144,83)        | 1.84 (2,227)         | 1.42 (11,227)        | 4.94* (24,235)        | 3.15* (132,118)      |
| Germany     | 2.64* (36,191)       | 1.89* (144,83)        | 2.60 (2,227)         | 1.59 (11,227)        | 1.71 (24,235)         | 2.22* (132,118)      |
| Greece      | 3.50* (36,191)       | 1.88* (144,83)        | 1.82 (2,227)         | 1.63 (11,227)        | 3.69* (24,235)        | 1.89* (132,118)      |
| Hungary     | 2.46* (36,191)       | 2.02* (144,83)        | 0.46 (2,227)         | 0.36 (11,227)        | 1.02 (24,235)         | 2.87* (132,118)      |
| Italy       | 1.84* (36,191)       | 1.91* (144,83)        | 3.69* (2,227)        | 6.80* (11,227)       | 1.06 (24,235)         | 2.62* (132,118)      |
| Japan       | 3.80* (36,195)       | 1.88* (144,87)        | 0.17 (2,231)         | 1.59 (11,231)        | 3.73* (24,235)        | 2.60* (132,118)      |
| Luxembourg  | 1.80* (36,191)       | 1.75* (144,83)        | 2.41 (2,227)         | 1.35 (11,227)        | 1.55 (24,235)         | 1.76* (132,118)      |
| Netherlands | 2.84* (36,191)       | 2.84* (144,83)        | 0.32 (2,227)         | 0.97 (11,227)        | 1.10 (24,235)         | 2.95* (132,118)      |
| Portugal    | 2.45* (36,191)       | 1.56* (144,83)        | 2.53 (2,227)         | 1.31 (11,227)        | 1.56 (24,235)         | 2.10* (132,118)      |
| Spain       | 2.23* (36,191)       | 2.05* (144,83)        | 0.48 (2,227)         | 0.97 (11,227)        | 4.61* (24,235)        | 4.44* (132,118)      |
| Sweden      | 3.15* (36,207)       | 2.24* (144,99)        | 3.57* (2,243)        | 2.73* (11,243)       | 3.02* (24,235)        | 5.82* (132,118)      |
| UK          | 2.46* (36,195)       | 2.35* (144,87)        | 0.92 (2,231)         | 1.72 (11,231)        | 1.41 (24,235)         | 3.21* (132,118)      |
| USA         | 1.76* (36,197)       | 1.74* (144,89)        | 1.12 (2,233)         | 1.21 (11,233)        | 7.37* (24,235)        | 1.30* (132,118)      |
| Euro Area   | 2.81* (36,191)       | 1.99* (144,83)        | 1.72 (2,227)         | 1.33 (11,227)        | 0.88 (24,235)         | 4.26* (132,118)      |

Note: \* denotes significant at the 5 % level; and  $F_{PeARI_{-12}}$  and  $F_{SH}$  represent the results of the Periodic residual autocorrelation tests of order 1 to 12, and the Seasonal heterocedasticity tests respectively.  $F_{PAR(\cdot)}$  denotes the F-test for  $H_0$  in (2.10) presented in Section 2.3. The values in brackets, (., .), indicate the degrees of freedom of the F-statistics.

**Table 5.3a:** Forecasts of Industrial Production

| Ranking | Austria |        |       |        |       |        |       |        | Canada |        |       |        |       |        |       |        | Germany |        |       |        |       |        |       |        | Denmark |        |       |        |       |        |       |        |     |        |     |        |    |        |
|---------|---------|--------|-------|--------|-------|--------|-------|--------|--------|--------|-------|--------|-------|--------|-------|--------|---------|--------|-------|--------|-------|--------|-------|--------|---------|--------|-------|--------|-------|--------|-------|--------|-----|--------|-----|--------|----|--------|
|         | h=1     |        | h=3   |        | h=8   |        | h=12  |        | h=1    |        | h=3   |        | h=8   |        | h=12  |        | h=1     |        | h=3   |        | h=8   |        | h=12  |        | h=1     |        | h=3   |        | h=8   |        | h=12  |        |     |        |     |        |    |        |
|         | RMSPE   | RMSPE  | RMSPE | RMSPE  | RMSPE | RMSPE  | RMSPE | RMSPE  | RMSPE  | RMSPE  | RMSPE | RMSPE  | RMSPE | RMSPE  | RMSPE | RMSPE  | RMSPE   | RMSPE  | RMSPE | RMSPE  | RMSPE | RMSPE  | RMSPE | RMSPE  | RMSPE   | RMSPE  | RMSPE | RMSPE  | RMSPE | RMSPE  | RMSPE |        |     |        |     |        |    |        |
| 1       | M11     | 0,0361 | M12   | 0,0447 | M6    | 0,0564 | M6    | 0,0568 | M1     | 0,0133 | C11   | 0,0159 | M1    | 0,0221 | M1    | 0,0271 | M17     | 0,0158 | M11   | 0,0203 | M11   | 0,0331 | M12   | 0,0340 | C10     | 0,0306 | C9    | 0,0306 | C10   | 0,0307 | C18   | 0,0303 |     |        |     |        |    |        |
| 2       | C1      | 0,0365 | M11   | 0,0454 | M7    | 0,0608 | M7    | 0,0592 | C1     | 0,0133 | C8    | 0,0164 | C14   | 0,0224 | M7    | 0,0280 | C3      | 0,0162 | M7    | 0,0203 | C9    | 0,0349 | M11   | 0,0341 | C9      | 0,0308 | C10   | 0,0308 | C5    | 0,0313 | M4    | 0,0316 |     |        |     |        |    |        |
| 3       | C3      | 0,0366 | M6    | 0,0459 | M12   | 0,0641 | M8    | 0,0665 | C3     | 0,0133 | M7    | 0,0171 | C12   | 0,0229 | C12   | 0,0283 | C8      | 0,0162 | C11   | 0,0219 | M7    | 0,0351 | C8    | 0,0351 | C7      | 0,0311 | M4    | 0,0308 | C4    | 0,0313 | C10   | 0,0319 |     |        |     |        |    |        |
| 4       | C17     | 0,0371 | M7    | 0,0464 | M8    | 0,0669 | M12   | 0,0696 | M11    | 0,0133 | M12   | 0,0171 | C17   | 0,0230 | C9    | 0,0289 | C17     | 0,0163 | C15   | 0,0222 | C17   | 0,0358 | C7    | 0,0356 | C8      | 0,0312 | C17   | 0,0308 | C15   | 0,0313 | C12   | 0,0323 |     |        |     |        |    |        |
| 5       | M12     | 0,0372 | C17   | 0,0468 | C10   | 0,0689 | C8    | 0,0721 | C17    | 0,0134 | M1    | 0,0171 | C7    | 0,0231 | C17   | 0,0292 | C16     | 0,0163 | C4    | 0,0222 | C16   | 0,0359 | C12   | 0,0356 | C6      | 0,0313 | C7    | 0,0309 | C6    | 0,0313 | C17   | 0,0323 |     |        |     |        |    |        |
| 6       | M6      | 0,0373 | C16   | 0,0471 | C16   | 0,0692 | M10   | 0,0743 | C16    | 0,0135 | C14   | 0,0171 | C16   | 0,0231 | C10   | 0,0295 | C1      | 0,0163 | C16   | 0,0222 | C7    | 0,0360 | C9    | 0,0357 | C5      | 0,0314 | C6    | 0,0309 | C7    | 0,0313 | C13   | 0,0324 |     |        |     |        |    |        |
| 7       | C16     | 0,0373 | C4    | 0,0474 | C4    | 0,0692 | C18   | 0,0761 | C14    | 0,0135 | C9    | 0,0171 | C6    | 0,0232 | C7    | 0,0295 | C4      | 0,0163 | C17   | 0,0222 | M12   | 0,0360 | C6    | 0,0359 | C11     | 0,0316 | C16   | 0,0309 | C16   | 0,0324 | C15   | 0,0316 |     |        |     |        |    |        |
| 8       | C15     | 0,0375 | C15   | 0,0474 | C15   | 0,0692 | C2    | 0,0764 | C4     | 0,0135 | C12   | 0,0173 | C9    | 0,0232 | C16   | 0,0296 | C15     | 0,0163 | C10   | 0,0222 | C6    | 0,0360 | C14   | 0,0361 | C4      | 0,0316 | C4    | 0,0310 | C14   | 0,0323 | C5    | 0,0324 |     |        |     |        |    |        |
| 9       | C4      | 0,0375 | C5    | 0,0475 | C17   | 0,0693 | M4    | 0,0765 | C15    | 0,0135 | C7    | 0,0175 | C5    | 0,0233 | M6    | 0,0297 | C5      | 0,0164 | C5    | 0,0222 | C5    | 0,0360 | C5    | 0,0361 | C16     | 0,0316 | C15   | 0,0310 | M4    | 0,0323 | C7    | 0,0313 | C13 | 0,0323 |     |        |    |        |
| 10      | C14     | 0,0376 | C14   | 0,0476 | C5    | 0,0695 | C11   | 0,0766 | C8     | 0,0136 | C16   | 0,0176 | C15   | 0,0234 | C14   | 0,0297 | C14     | 0,0164 | C8    | 0,0223 | C14   | 0,0360 | C17   | 0,0362 | C17     | 0,0317 | C14   | 0,0318 | C8    | 0,0324 | C15   | 0,0325 |     |        |     |        |    |        |
| 11      | C10     | 0,0377 | C10   | 0,0476 | C6    | 0,0697 | C15   | 0,0766 | C5     | 0,0136 | C6    | 0,0176 | C4    | 0,0234 | C6    | 0,0298 | C6      | 0,0164 | C6    | 0,0223 | C4    | 0,0360 | C16   | 0,0363 | C13     | 0,0318 | C8    | 0,0318 | C9    | 0,0326 | C4    | 0,0325 | M4  | 0,0321 | C17 | 0,0333 | C9 | 0,0326 |
| 12      | C5      | 0,0377 | C6    | 0,0476 | M10   | 0,0699 | C4    | 0,0766 | C6     | 0,0136 | C5    | 0,0176 | C13   | 0,0239 | M8    | 0,0298 | C10     | 0,0164 | C7    | 0,0223 | C15   | 0,0360 | C4    | 0,0364 | C13     | 0,0318 | C8    | 0,0318 | C9    | 0,0326 | C4    | 0,0325 | C14 | 0,0330 |     |        |    |        |
| 13      | C6      | 0,0378 | C7    | 0,0478 | C2    | 0,0700 | C16   | 0,0767 | C7     | 0,0136 | C4    | 0,0176 | C11   | 0,0239 | C13   | 0,0298 | C7      | 0,0164 | C14   | 0,0224 | C10   | 0,0361 | C15   | 0,0364 | M4      | 0,0321 | C17   | 0,0321 | C13   | 0,0333 | C9    | 0,0326 | C16 | 0,0316 |     |        |    |        |
| 14      | C7      | 0,0380 | C2    | 0,0483 | C7    | 0,0701 | C17   | 0,0767 | C12    | 0,0136 | C15   | 0,0176 | C10   | 0,0240 | C5    | 0,0299 | C11     | 0,0166 | M4    | 0,0227 | C12   | 0,0362 | C10   | 0,0367 | C14     | 0,0326 | C12   | 0,0326 | C13   | 0,0325 | M4    | 0,0323 | C7  | 0,0324 | C14 | 0,0330 |    |        |
| 15      | C2      | 0,0382 | C9    | 0,0486 | C14   | 0,0705 | C5    | 0,0767 | C9     | 0,0136 | C13   | 0,0176 | C2    | 0,0242 | C8    | 0,0300 | M4      | 0,0166 | C12   | 0,0227 | C8    | 0,0364 | M4    | 0,0367 | C12     | 0,0326 | C13   | 0,0327 | C11   | 0,0330 | C11   | 0,0334 | C11 | 0,0334 | C15 | 0,0335 |    |        |
| 16      | C13     | 0,0385 | C13   | 0,0489 | M4    | 0,0705 | C10   | 0,0769 | C11    | 0,0136 | C17   | 0,0176 | C8    | 0,0244 | C4    | 0,0301 | C9      | 0,0167 | C13   | 0,0227 | M1    | 0,0367 | C11   | 0,0369 | C2      | 0,0327 | C11   | 0,0330 | C11   | 0,0344 | M17   | 0,0335 | C2  | 0,0345 | C2  | 0,0336 |    |        |
| 17      | M2      | 0,0385 | C12   | 0,0494 | M3    | 0,0710 | M3    | 0,0769 | C13    | 0,0137 | C10   | 0,0177 | M6    | 0,0255 | C15   | 0,0301 | C13     | 0,0168 | C9    | 0,0228 | M4    | 0,0370 | C13   | 0,0370 | M17     | 0,0339 | C2    | 0,0336 | C2    | 0,0345 | C2    | 0,0336 | C17 | 0,0339 | C18 | 0,0357 |    |        |
| 18      | M3      | 0,0386 | M3    | 0,0497 | C11   | 0,0711 | C6    | 0,0769 | C10    | 0,0137 | C2    | 0,0178 | M11   | 0,0255 | M3    | 0,0305 | C2      | 0,0168 | C2    | 0,0229 | C2    | 0,0375 | C2    | 0,0374 | M12     | 0,0353 | C18   | 0,0357 | C18   | 0,0362 | C8    | 0,0344 | M10 | 0,0358 |     |        |    |        |
| 19      | C8      | 0,0387 | C11   | 0,0497 | M2    | 0,0712 | C7    | 0,0771 | M7     | 0,0137 | M11   | 0,0182 | M8    | 0,0255 | C2    | 0,0307 | C12     | 0,0169 | M17   | 0,0229 | M8    | 0,0375 | M2    | 0,0380 | C18     | 0,0356 | M3    | 0,0367 | M3    | 0,0366 | M10   | 0,0358 | C18 | 0,0356 | M3  | 0,0367 |    |        |
| 20      | C11     | 0,0387 | M2    | 0,0497 | C13   | 0,0712 | M2    | 0,0771 | C2     | 0,0139 | M6    | 0,0183 | M7    | 0,0256 | C11   | 0,0309 | C18     | 0,0171 | M1    | 0,0231 | C13   | 0,0379 | M1    | 0,0383 | M8      | 0,0357 | M2    | 0,0369 | M2    | 0,0367 | M11   | 0,0365 | C12 | 0,0326 | C13 | 0,0327 |    |        |
| 21      | C9      | 0,0388 | C8    | 0,0499 | C18   | 0,0713 | C14   | 0,0781 | M6     | 0,0143 | M17   | 0,0192 | M12   | 0,0256 | M11   | 0,0323 | M10     | 0,0176 | M3    | 0,0234 | M2    | 0,0380 | M6    | 0,0384 | M5      | 0,0359 | M15   | 0,0373 | M16   | 0,0383 | M3    | 0,0372 | C15 | 0,0379 |     |        |    |        |
| 22      | C12     | 0,0390 | M4    | 0,0502 | C9    | 0,0719 | C13   | 0,0789 | M12    | 0,0143 | M10   | 0,0195 | M17   | 0,0282 | M2    | 0,0326 | M5      | 0,0177 | M6    | 0,0238 | M6    | 0,0390 | M8    | 0,0384 | M15     | 0,0379 | M14   | 0,0380 | M6    | 0,0385 | M2    | 0,0373 | C16 | 0,0379 |     |        |    |        |
| 23      | M7      | 0,0392 | M5    | 0,0504 | C8    | 0,0720 | C9    | 0,0803 | M17    | 0,0145 | M8    | 0,0197 | M3    | 0,0283 | M4    | 0,0346 | M3      | 0,0178 | M10   | 0,0242 | C11   | 0,0390 | M7    | 0,0397 | M3      | 0,0379 | M16   | 0,0380 | M15   | 0,0388 | M6    | 0,0388 | C15 | 0,0388 |     |        |    |        |
| 24      | M4      | 0,0394 | M17   | 0,0505 | C12   | 0,0726 | C12   | 0,0835 | M10    | 0,0148 | C3    | 0,0204 | M2    | 0,0287 | M17   | 0,0349 | M1      | 0,0178 | M16   | 0,0247 | M17   | 0,0405 | M3    | 0,0416 | M16     | 0,0381 | M10   | 0,0387 | M14   | 0,0393 | M16   | 0,0399 | C16 | 0,0381 |     |        |    |        |
| 25      | M17     | 0,0398 | C3    | 0,0508 | M11   | 0,0726 | M11   | 0,0844 | M4     | 0,0149 | C1    | 0,0210 | M4    | 0,0288 | M12   | 0,0358 | M2      | 0,0181 | M2    | 0,0256 | M3    | 0,0405 | M17   | 0,0441 | M2      | 0,0389 | M12   | 0,0389 | M11   | 0,0395 | M14   | 0,0403 | C16 | 0,0389 |     |        |    |        |
| 26      | M14     | 0,0398 | C1    | 0,0519 | M5    | 0,0728 | M5    | 0,0864 | C18    | 0,0155 | M4    | 0,0214 | C18   | 0,0303 | M14   | 0,0389 | M11     | 0,0181 | M15   | 0,0256 | M10   | 0,0415 | M14   | 0,0450 | M14     | 0,0391 | M6    | 0,0391 | M7    | 0,0399 | M15   | 0,0413 | C18 | 0,0391 |     |        |    |        |
| 27      | M16     | 0,0399 | M16   | 0,0522 | M17   | 0,0779 | M17   | 0,0908 | M8     | 0,0157 | M2    | 0,0214 | M10   | 0,0307 | M10   | 0,0393 | M16     | 0,0184 | M14   | 0,0257 | M14   | 0,0427 | M10   | 0,0450 | M7      | 0,0393 | M8    | 0,0392 | M10   | 0,0404 | M8    | 0,0414 | C18 | 0,0393 |     |        |    |        |
| 28      | M15     | 0,0401 | M14   | 0,0525 | M16   | 0,0791 | M14   | 0,0912 | M3     | 0,0159 | M3    | 0,0223 | M14   | 0,0324 | M5    | 0,0417 | M15     | 0,0186 | C3    | 0,0258 | M16   | 0,0436 | M16   | 0,0470 | M10     | 0,0395 | M1    | 0,0395 | M8    | 0,0406 | M7    | 0,0447 | C18 | 0,0395 |     |        |    |        |
| 29      | M1      | 0,0403 | M1    | 0,0530 | M14   | 0,0792 | M16   | 0,0913 | M2     | 0,0162 | M14   | 0,0225 | C3    | 0,0334 | M16   | 0,0463 | M14     | 0,0186 | C1    | 0,0266 | M5    | 0,0459 | M5    | 0,0477 | M6      | 0,0402 | M7    | 0,0408 | M12   | 0,0431 | M5    | 0,0464 | C18 | 0,0395 |     |        |    |        |
| 30      | M10     | 0,0406 | C18   | 0,0531 | M15   | 0,0798 | M15   | 0,0915 | M14    | 0,0163 | M5    | 0,0234 | M5    | 0,0336 | M15   | 0,0487 | M6      | 0,0186 | M12   | 0,0266 | C3    | 0,0463 | M15   | 0,0526 | M1      | 0,0415 | M11   | 0,0430 | M1    | 0,0434 | M1    | 0,0494 | C18 | 0,0395 |     |        |    |        |
| 31      | C18     | 0,0417 | M15   | 0,0534 | M1    | 0,0810 | M1    | 0,0928 | M15    | 0,0165 | C18   | 0,0243 | C1    | 0,0352 | C3    | 0,0496 | M7      | 0,0186 | C18   | 0,0271 | M15   | 0,0471 | C3    | 0,0603 | M11     | 0,0417 | M5    | 0,0464 | M5    | 0,0502 | M12   | 0,0538 | C18 | 0,0395 |     |        |    |        |
| 32      | M5      | 0,0438 | M8    | 0,0535 | C3    | 0,1065 | C3    | 0,1375 | M16    | 0,0169 | M16   | 0,0251 | M16   | 0,0378 | M9    | 0,0519 | M12     | 0,0197 | M5    | 0,0276 | C1    | 0,0483 | C1    | 0,0644 | M13     | 0,0848 | C3    | 0,0841 | C3    | 0,0887 | C3    | 0,1062 | C18 | 0,0395 |     |        |    |        |
| 33      | M8      | 0,0455 | M10   | 0,0539 | C1    | 0,1126 | C1    | 0,1474 | M5     | 0,0179 | M15   | 0,0251 | M15   | 0,0386 | C1    | 0,0531 | M8      | 0,0218 | M8    | 0,0304 | C18   | 0,0188 | M18   | 0,0637 | C18     | 0,0749 | C3    | 0,0857 | C1    | 0,0928 | C1    | 0,0976 | C1  | 0,1175 | M13 | 0,1377 | M9 | 1,3468 |
| 34      | M9      | 0,0612 | M9    | 0,1834 | M9    | 0,8138 | M9    | 1,1111 | M9     | 0,0218 | M9    | 0,0636 | M9    | 0,0453 | C18   | 0,0542 | M9      | 0,0248 | M9    | 0,0874 | M9    | 0,0755 | M9    | 0,0826 | C1      | 0,0942 | M13   | 0,2025 | M13   | 0,6171 | M13   | 1,0681 | C18 | 0,0542 |     |        |    |        |
| 35      | M13     | 0,0791 | M13   | 0,3021 | M13   | 0,8378 | M13   | 1,3664 | M13    | 0,0244 | M13   | 0,1536 | M13   | 0,4048 | M13   | 0,6554 | M13     | 0,0264 | M13   | 0,1828 | M13   | 0,4735 | M13   | 0,7469 | M9      |        |       |        |       |        |       |        |     |        |     |        |    |        |

**Table 5.3b: Forecasts of Industrial Production**

| Ranking | Euro Area |        |       |        |       |        |       |        | Spain |        |       |        |       |        |       |        | Finland |        |       |        |       |        |       |        | France |        |       |        |       |        |      |        |
|---------|-----------|--------|-------|--------|-------|--------|-------|--------|-------|--------|-------|--------|-------|--------|-------|--------|---------|--------|-------|--------|-------|--------|-------|--------|--------|--------|-------|--------|-------|--------|------|--------|
|         | h=1       |        | h=3   |        | h=8   |        | h=12  |        | h=1   |        | h=3   |        | h=8   |        | h=12  |        | h=1     |        | h=3   |        | h=8   |        | h=12  |        | h=1    |        | h=3   |        | h=8   |        | h=12 |        |
|         | RMSPE     | RMSPE  | RMSPE | RMSPE  | RMSPE | RMSPE  | RMSPE | RMSPE  | RMSPE | RMSPE  | RMSPE | RMSPE  | RMSPE | RMSPE  | RMSPE | RMSPE  | RMSPE   | RMSPE  | RMSPE | RMSPE  | RMSPE | RMSPE  | RMSPE | RMSPE  | RMSPE  | RMSPE  | RMSPE | RMSPE  | RMSPE | RMSPE  |      |        |
| 1       | M11       | 0,0180 | M11   | 0,0293 | M11   | 0,0548 | C11   | 0,0569 | C17   | 0,0178 | C10   | 0,0204 | C8    | 0,0252 | M11   | 0,0229 | M17     | 0,0570 | M17   | 0,0805 | M17   | 0,1230 | M3    | 0,1433 | M6     | 0,0255 | C18   | 0,0227 | C18   | 0,0268 | M7   | 0,0295 |
| 2       | M7        | 0,0197 | M7    | 0,0295 | C9    | 0,0555 | C8    | 0,0571 | C4    | 0,0178 | C15   | 0,0206 | C9    | 0,0256 | C9    | 0,0243 | C10     | 0,0577 | C15   | 0,0835 | M1    | 0,1290 | M2    | 0,1442 | C8     | 0,0264 | M6    | 0,0260 | M6    | 0,0278 | C18  | 0,0298 |
| 3       | M12       | 0,0203 | C10   | 0,0314 | C14   | 0,0555 | C7    | 0,0588 | C15   | 0,0178 | C4    | 0,0206 | C7    | 0,0261 | C8    | 0,0245 | C13     | 0,0590 | C4    | 0,0835 | C4    | 0,1298 | M17   | 0,1445 | C11    | 0,0267 | C8    | 0,0264 | C8    | 0,0281 | M8   | 0,0316 |
| 4       | C16       | 0,0211 | M12   | 0,0316 | C7    | 0,0556 | C14   | 0,0593 | C16   | 0,0178 | C5    | 0,0206 | M11   | 0,0262 | C7    | 0,0249 | C11     | 0,0596 | M1    | 0,0837 | C15   | 0,1298 | C8    | 0,1457 | C18    | 0,0269 | M12   | 0,0276 | C11   | 0,0282 | C9   | 0,0316 |
| 5       | C15       | 0,0211 | M10   | 0,0316 | C6    | 0,0557 | C6    | 0,0595 | C5    | 0,0179 | C8    | 0,0206 | C6    | 0,0262 | C6    | 0,0252 | C7      | 0,0596 | C16   | 0,0838 | C5    | 0,1301 | M1    | 0,1461 | C14    | 0,0269 | C9    | 0,0276 | M10   | 0,0288 | M12  | 0,0323 |
| 6       | C4        | 0,0211 | C15   | 0,0320 | C16   | 0,0557 | C9    | 0,0596 | C8    | 0,0179 | C6    | 0,0207 | C5    | 0,0262 | C5    | 0,0253 | C9      | 0,0597 | C17   | 0,0839 | C6    | 0,1305 | C7    | 0,1467 | C7     | 0,0274 | C11   | 0,0277 | M7    | 0,0291 | C8   | 0,0325 |
| 7       | C17       | 0,0212 | C4    | 0,0320 | C5    | 0,0557 | C17   | 0,0597 | C6    | 0,0179 | C16   | 0,0207 | C15   | 0,0262 | C4    | 0,0254 | C8      | 0,0598 | C5    | 0,0839 | C14   | 0,1309 | C6    | 0,1468 | C9     | 0,0274 | C7    | 0,0280 | C7    | 0,0296 | C12  | 0,0325 |
| 8       | C5        | 0,0212 | C16   | 0,0320 | C4    | 0,0558 | C5    | 0,0599 | C9    | 0,0179 | C7    | 0,0207 | C4    | 0,0262 | C15   | 0,0254 | C2      | 0,0599 | C14   | 0,0841 | C16   | 0,1309 | C5    | 0,1468 | C6     | 0,0275 | C6    | 0,0282 | C9    | 0,0298 | M6   | 0,0327 |
| 9       | M10       | 0,0212 | C17   | 0,0321 | C15   | 0,0558 | C16   | 0,0600 | C7    | 0,0179 | C17   | 0,0207 | C16   | 0,0265 | C16   | 0,0255 | M4      | 0,0600 | C6    | 0,0842 | C7    | 0,1310 | C4    | 0,1469 | C5     | 0,0275 | C10   | 0,0282 | C6    | 0,0298 | C11  | 0,0333 |
| 10      | C10       | 0,0212 | C5    | 0,0322 | C17   | 0,0558 | M3    | 0,0601 | C10   | 0,0180 | C14   | 0,0207 | C10   | 0,0268 | C12   | 0,0256 | M10     | 0,0601 | C7    | 0,0847 | C17   | 0,1319 | C15   | 0,1469 | C4     | 0,0275 | C5    | 0,0283 | C5    | 0,0300 | C7   | 0,0337 |
| 11      | C6        | 0,0213 | C2    | 0,0322 | M7    | 0,0559 | C4    | 0,0604 | C13   | 0,0180 | C11   | 0,0208 | C17   | 0,0268 | C17   | 0,0258 | C12     | 0,0601 | C18   | 0,0853 | C10   | 0,1322 | C14   | 0,1474 | C15    | 0,0275 | C4    | 0,0284 | C10   | 0,0300 | C6   | 0,0340 |
| 12      | C7        | 0,0214 | C11   | 0,0323 | C8    | 0,0562 | C15   | 0,0604 | C2    | 0,0181 | C13   | 0,0210 | C11   | 0,0269 | C10   | 0,0258 | M5      | 0,0601 | C10   | 0,0855 | M3    | 0,1323 | C16   | 0,1479 | C16    | 0,0276 | C15   | 0,0284 | C4    | 0,0302 | C5   | 0,0341 |
| 13      | C11       | 0,0216 | C6    | 0,0323 | M3    | 0,0564 | C10   | 0,0616 | C12   | 0,0181 | C9    | 0,0212 | M12   | 0,0269 | C14   | 0,0264 | C14     | 0,0603 | C11   | 0,0870 | M12   | 0,1328 | C9    | 0,1480 | C10    | 0,0277 | C16   | 0,0285 | C15   | 0,0302 | C17  | 0,0341 |
| 14      | C2        | 0,0218 | M3    | 0,0323 | C10   | 0,0565 | M2    | 0,0621 | C14   | 0,0181 | C2    | 0,0212 | C12   | 0,0274 | C13   | 0,0265 | C6      | 0,0605 | C2    | 0,0871 | M2    | 0,1330 | C17   | 0,1487 | C17    | 0,0277 | C14   | 0,0285 | C16   | 0,0302 | C16  | 0,0341 |
| 15      | C13       | 0,0220 | C14   | 0,0323 | M12   | 0,0569 | M8    | 0,0630 | C11   | 0,0182 | C12   | 0,0213 | M4    | 0,0277 | C11   | 0,0266 | M1      | 0,0608 | C13   | 0,0873 | C8    | 0,1336 | C10   | 0,1491 | C12    | 0,0279 | C17   | 0,0286 | C17   | 0,0302 | C10  | 0,0342 |
| 16      | M17       | 0,0220 | C7    | 0,0325 | C2    | 0,0575 | C12   | 0,0632 | M4    | 0,0187 | M4    | 0,0219 | C14   | 0,0277 | C2    | 0,0266 | C17     | 0,0608 | C12   | 0,0875 | C11   | 0,1337 | C2    | 0,1507 | M8     | 0,0282 | M8    | 0,0287 | M12   | 0,0304 | C15  | 0,0343 |
| 17      | M3        | 0,0222 | C13   | 0,0326 | M10   | 0,0576 | C2    | 0,0638 | M2    | 0,0189 | M11   | 0,0221 | C2    | 0,0279 | M4    | 0,0267 | M2      | 0,0610 | M3    | 0,0879 | M4    | 0,1340 | C11   | 0,1510 | M10    | 0,0282 | C12   | 0,0289 | C12   | 0,0309 | C4   | 0,0343 |
| 18      | C8        | 0,0222 | C8    | 0,0327 | C11   | 0,0576 | M12   | 0,0641 | M17   | 0,0190 | M17   | 0,0221 | C18   | 0,0279 | M2    | 0,0271 | M3      | 0,0611 | C9    | 0,0880 | C13   | 0,1356 | M8    | 0,1510 | M5     | 0,0285 | C13   | 0,0293 | M4    | 0,0309 | M11  | 0,0344 |
| 19      | C9        | 0,0223 | C9    | 0,0331 | C12   | 0,0577 | C13   | 0,0642 | M11   | 0,0190 | M3    | 0,0225 | C13   | 0,0281 | M12   | 0,0277 | C5      | 0,0614 | C8    | 0,0881 | C18   | 0,1356 | C12   | 0,1512 | C13    | 0,0286 | M7    | 0,0294 | M17   | 0,0314 | C14  | 0,0352 |
| 20      | C12       | 0,0224 | C12   | 0,0332 | C13   | 0,0579 | M7    | 0,0644 | M3    | 0,0192 | M12   | 0,0225 | M2    | 0,0282 | M3    | 0,0279 | C16     | 0,0614 | M16   | 0,0881 | C2    | 0,1360 | C13   | 0,1513 | C2     | 0,0286 | C2    | 0,0294 | C13   | 0,0314 | C2   | 0,0357 |
| 21      | M4        | 0,0225 | M4    | 0,0335 | M2    | 0,0585 | M1    | 0,0653 | M15   | 0,0194 | M2    | 0,0226 | M3    | 0,0287 | M17   | 0,0295 | M16     | 0,0619 | M2    | 0,0883 | C9    | 0,1367 | M4    | 0,1520 | M4     | 0,0288 | M4    | 0,0300 | C14   | 0,0318 | C13  | 0,0358 |
| 22      | C14       | 0,0225 | M17   | 0,0337 | M1    | 0,0585 | M4    | 0,0660 | M12   | 0,0194 | C18   | 0,0233 | M17   | 0,0290 | M8    | 0,0296 | M15     | 0,0624 | M4    | 0,0886 | C12   | 0,1374 | M11   | 0,1523 | M12    | 0,0297 | M10   | 0,0302 | C2    | 0,0321 | M10  | 0,0361 |
| 23      | M1        | 0,0228 | M1    | 0,0340 | M8    | 0,0600 | M11   | 0,0661 | C18   | 0,0194 | M14   | 0,0233 | M1    | 0,0309 | M1    | 0,0313 | C4      | 0,0625 | M12   | 0,0888 | M11   | 0,1378 | M12   | 0,1574 | M17    | 0,0298 | M11   | 0,0309 | M8    | 0,0322 | M1   | 0,0368 |
| 24      | M2        | 0,0229 | M15   | 0,0347 | M4    | 0,0610 | M10   | 0,0695 | M14   | 0,0194 | M1    | 0,0235 | M15   | 0,0326 | M15   | 0,0333 | C15     | 0,0625 | M10   | 0,0891 | C3    | 0,1399 | M16   | 0,1617 | M11    | 0,0300 | M17   | 0,0313 | M11   | 0,0333 | M3   | 0,0383 |
| 25      | M15       | 0,0232 | M16   | 0,0352 | M17   | 0,0612 | M17   | 0,0704 | M10   | 0,0200 | M15   | 0,0236 | M14   | 0,0326 | M14   | 0,0336 | M14     | 0,0626 | M15   | 0,0899 | M16   | 0,1423 | M5    | 0,1639 | M7     | 0,0303 | M1    | 0,0326 | M1    | 0,0340 | M2   | 0,0388 |
| 26      | M14       | 0,0234 | M2    | 0,0357 | M6    | 0,0637 | M6    | 0,0705 | M16   | 0,0201 | M16   | 0,0240 | M8    | 0,0329 | M5    | 0,0346 | C18     | 0,0638 | M11   | 0,0908 | C1    | 0,1427 | M7    | 0,1657 | M16    | 0,0326 | M2    | 0,0328 | M3    | 0,0341 | M4   | 0,0395 |
| 27      | M16       | 0,0235 | M14   | 0,0357 | M14   | 0,0637 | M14   | 0,0711 | M6    | 0,0206 | M5    | 0,0262 | M7    | 0,0330 | C18   | 0,0349 | M12     | 0,0638 | M14   | 0,0916 | M10   | 0,1429 | M14   | 0,1657 | M2     | 0,0331 | M16   | 0,0334 | M2    | 0,0355 | M17  | 0,0402 |
| 28      | M5        | 0,0241 | M6    | 0,0366 | M15   | 0,0654 | M5    | 0,0725 | M1    | 0,0207 | M10   | 0,0263 | M16   | 0,0333 | M16   | 0,0351 | M13     | 0,0648 | M5    | 0,0922 | M15   | 0,1466 | M15   | 0,1667 | M15    | 0,0335 | M14   | 0,0345 | M16   | 0,0371 | M5   | 0,0425 |
| 29      | M6        | 0,0241 | M5    | 0,0369 | M5    | 0,0661 | M15   | 0,0740 | M5    | 0,0209 | M7    | 0,0263 | M5    | 0,0356 | M7    | 0,0362 | M11     | 0,0662 | C3    | 0,0983 | M14   | 0,1467 | M10   | 0,1671 | M1     | 0,0336 | M15   | 0,0346 | M15   | 0,0373 | M16  | 0,0447 |
| 30      | C18       | 0,0245 | M8    | 0,0404 | M16   | 0,0670 | M16   | 0,0766 | M7    | 0,0215 | M6    | 0,0267 | M10   | 0,0365 | M10   | 0,0371 | M6      | 0,0679 | C1    | 0,1026 | M5    | 0,1468 | C3    | 0,1687 | M14    | 0,0345 | M3    | 0,0346 | M14   | 0,0379 | M14  | 0,0459 |
| 31      | M8        | 0,0252 | C18   | 0,0441 | C18   | 0,1139 | C3    | 0,1414 | M13   | 0,0226 | M8    | 0,0300 | M6    | 0,0396 | M6    | 0,0456 | C3      | 0,0724 | M6    | 0,1050 | M7    | 0,1481 | C18   | 0,1694 | M3     | 0,0349 | M5    | 0,0421 | M5    | 0,0417 | M15  | 0,0469 |
| 32      | M13       | 0,0293 | C3    | 0,0922 | C3    | 0,1189 | C18   | 0,1448 | M8    | 0,0233 | C3    | 0,0794 | C3    | 0,1372 | C3    | 0,1498 | C1      | 0,0757 | M7    | 0,1060 | M8    | 0,1592 | C1    | 0,1739 | M13    | 0,0435 | C3    | 0,0871 | C3    | 0,1183 | C3   | 0,1514 |
| 33      | C3        | 0,1000 | C1    | 0,1018 | C1    | 0,1297 | C1    | 0,1543 | C3    | 0,1053 | C1    | 0,0884 | C1    | 0,1526 | C1    | 0,1669 | M7      | 0,0790 | M8    | 0,1119 | M6    |        |       |        |        |        |       |        |       |        |      |        |

**Table 5.3c: Forecasts of Industrial Production**

| Ranking | UK           |              |              |               | Greece       |              |              |               | Hungary      |              |              |               | Italy        |              |              |               |
|---------|--------------|--------------|--------------|---------------|--------------|--------------|--------------|---------------|--------------|--------------|--------------|---------------|--------------|--------------|--------------|---------------|
|         | h=1<br>RMSPE | h=3<br>RMSPE | h=8<br>RMSPE | h=12<br>RMSPE |
| 1       | C18 0,0220   | C18 0,0233   | M7 0,0286    | M8 0,0274     | M17 0,0299   | M10 0,0343   | M10 0,0403   | C18 0,0411    | C10 0,0297   | M1 0,0326    | M1 0,0397    | M1 0,0366     | C18 0,0206   | M1 0,0202    | M3 0,0239    | C2 0,0236     |
| 2       | M12 0,0228   | M12 0,0239   | M8 0,0293    | M7 0,0291     | C8 0,0302    | C10 0,0346   | C11 0,0414   | M7 0,0417     | C3 0,0297    | C6 0,0332    | C9 0,0411    | C8 0,0387     | M5 0,0213    | M17 0,0205   | C2 0,0240    | C13 0,0240    |
| 3       | M6 0,0230    | M7 0,0242    | M12 0,0316   | M12 0,0329    | C10 0,0303   | C8 0,0346    | C18 0,0415   | M12 0,0434    | C17 0,0298   | C2 0,0332    | C10 0,0415   | M8 0,0396     | C14 0,0218   | C8 0,0206    | M2 0,0240    | M3 0,0241     |
| 4       | C8 0,0237    | M8 0,0247    | M6 0,0329    | C18 0,0373    | C11 0,0304   | C13 0,0346   | C10 0,0417   | M11 0,0439    | C15 0,0298   | C5 0,0332    | C15 0,0416   | C7 0,0399     | C11 0,0220   | C11 0,0207   | C13 0,0240   | M2 0,0241     |
| 5       | M10 0,0238   | C9 0,0247    | C10 0,0333   | M11 0,0393    | M5 0,0305    | C15 0,0347   | C15 0,0420   | M10 0,0444    | C4 0,0298    | C10 0,0332   | C4 0,0416    | C6 0,0400     | C8 0,0221    | C2 0,0209    | M1 0,0242    | M1 0,0246     |
| 6       | M11 0,0240   | C14 0,0251   | M10 0,0334   | M6 0,0401     | C7 0,0306    | C4 0,0347    | C4 0,0420    | M6 0,0449     | C16 0,0298   | C7 0,0332    | C5 0,0416    | C4 0,0400     | C4 0,0221    | C13 0,0210   | C14 0,0244   | C12 0,0248    |
| 7       | C14 0,0241   | C7 0,0251    | C8 0,0336    | C4 0,0416     | C6 0,0307    | C5 0,0347    | C16 0,0420   | M8 0,0457     | C5 0,0298    | C15 0,0332   | C6 0,0417    | C15 0,0400    | C15 0,0221   | C12 0,0211   | C12 0,0245   | C17 0,0261    |
| 8       | C9 0,0242    | C6 0,0252    | C14 0,0339   | C15 0,0416    | C13 0,0307   | C16 0,0347   | C8 0,0420    | M1 0,0457     | C1 0,0298    | C4 0,0332    | C7 0,0417    | C5 0,0400     | C4 0,0222    | C7 0,0212    | C17 0,0252   | M10 0,0263    |
| 9       | C7 0,0244    | C5 0,0253    | C4 0,0342    | C14 0,0417    | C5 0,0307    | C6 0,0348    | C5 0,0421    | C10 0,0457    | C6 0,0298    | C17 0,0333   | C17 0,0419   | C9 0,0403     | C16 0,0222   | C10 0,0212   | C16 0,0252   | C10 0,0263    |
| 10      | C10 0,0245   | C4 0,0253    | C15 0,0342   | C5 0,0418     | C15 0,0308   | C17 0,0348   | C17 0,0421   | C15 0,0460    | C7 0,0299    | C16 0,0333   | C16 0,0420   | C10 0,0404    | C5 0,0222    | C6 0,0212    | C9 0,0253    | C16 0,0263    |
| 11      | M7 0,0245    | C15 0,0253   | C5 0,0342    | C6 0,0419     | C4 0,0308    | M17 0,0349   | M6 0,0421    | C4 0,0460     | C2 0,0300    | C13 0,0335   | C11 0,0425   | C16 0,0409    | C17 0,0222   | C5 0,0212    | C4 0,0253    | M12 0,0263    |
| 12      | C6 0,0245    | C16 0,0254   | C18 0,0342   | C7 0,0422     | C16 0,0308   | C7 0,0349    | C6 0,0422    | C16 0,0461    | C13 0,0300   | C8 0,0339    | C8 0,0426    | C14 0,0413    | C6 0,0222    | C15 0,0212   | C15 0,0253   | C15 0,0266    |
| 13      | C12 0,0246   | C8 0,0254    | C6 0,0343    | C10 0,0425    | C17 0,0308   | C2 0,0350    | C2 0,0422    | C5 0,0462     | C12 0,0301   | C12 0,0339   | C12 0,0427   | C17 0,0413    | C7 0,0223    | C4 0,0212    | C10 0,0254   | C4 0,0266     |
| 14      | C5 0,0246    | C17 0,0255   | C7 0,0344    | C16 0,0426    | M10 0,0308   | C14 0,0353   | C13 0,0422   | C8 0,0462     | C11 0,0302   | C14 0,0339   | C2 0,0429    | M10 0,0418    | C10 0,0224   | C16 0,0212   | C5 0,0255    | C5 0,0269     |
| 15      | C11 0,0246   | M6 0,0255    | C16 0,0346   | C2 0,0428     | M4 0,0311    | C11 0,0354   | M1 0,0423    | M2 0,0463     | C9 0,0303    | C9 0,0340    | C13 0,0431   | C11 0,0421    | M1 0,0227    | M3 0,0213    | C6 0,0256    | C6 0,0271     |
| 16      | C4 0,0247    | C10 0,0257   | C17 0,0347   | C9 0,0429     | C9 0,0312    | C9 0,0358    | C7 0,0423    | C6 0,0463     | C8 0,0305    | C11 0,0347   | C14 0,0435   | C2 0,0431     | C2 0,0228    | C17 0,0213   | C7 0,0257    | C14 0,0272    |
| 17      | C15 0,0247   | C12 0,0258   | C11 0,0350   | C17 0,0431    | C14 0,0313   | M1 0,0359    | M7 0,0428    | C17 0,0464    | C14 0,0305   | M14 0,0350   | M10 0,0448   | C13 0,0435    | C13 0,0228   | C9 0,0213    | M12 0,0261   | C7 0,0274     |
| 18      | C17 0,0247   | C11 0,0258   | M11 0,0355   | M1 0,0434     | C12 0,0316   | C12 0,0360   | C14 0,0430   | C7 0,0466     | M11 0,0306   | M17 0,0352   | M8 0,0449    | C12 0,0447    | C9 0,0229    | M16 0,0215   | M17 0,0270   | M5 0,0278     |
| 19      | C16 0,0247   | M10 0,0259   | C9 0,0358    | C11 0,0443    | M6 0,0316    | M3 0,0360    | M2 0,0430    | C2 0,0468     | M17 0,0314   | C3 0,0353    | M14 0,0455   | M7 0,0448     | M12 0,0230   | C14 0,0217   | M14 0,0274   | M4 0,0283     |
| 20      | C3 0,0250    | M4 0,0266    | C13 0,0365   | C8 0,0443     | M1 0,0318    | M2 0,0364    | M3 0,0433    | C11 0,0469    | M10 0,0316   | M16 0,0354   | M16 0,0460   | M14 0,0471    | C12 0,0232   | M2 0,0218    | M10 0,0275   | C9 0,0284     |
| 21      | C1 0,0250    | C2 0,0269    | C2 0,0365    | M10 0,0446    | C2 0,0319    | M4 0,0365    | C12 0,0437   | M3 0,0471     | M1 0,0317    | M15 0,0354   | M15 0,0461   | M17 0,0472    | M16 0,0235   | M4 0,0221    | M16 0,0275   | C18 0,0295    |
| 22      | C13 0,0252   | C13 0,0269   | C12 0,0374   | C12 0,0447    | C18 0,0320   | M7 0,0367    | C9 0,0438    | C14 0,0472    | M2 0,0321    | M2 0,0356    | M2 0,0465    | M16 0,0477    | M17 0,0236   | M14 0,0222   | M15 0,0277   | M17 0,0301    |
| 23      | M8 0,0252    | M11 0,0269   | M4 0,0376    | M3 0,0451     | M2 0,0331    | M6 0,0368    | M5 0,0440    | C9 0,0480     | M14 0,0322   | C1 0,0358    | M17 0,0467   | M15 0,0479    | M2 0,0238    | M15 0,0224   | M5 0,0278    | M14 0,0310    |
| 24      | C2 0,0259    | C3 0,0277    | M1 0,0384    | C13 0,0453    | M3 0,0341    | C18 0,0373   | M4 0,0441    | C13 0,0480    | M16 0,0323   | M11 0,0359   | M11 0,0482   | M2 0,0489     | M3 0,0240    | C18 0,0230   | M4 0,0288    | C11 0,0314    |
| 25      | M17 0,0261   | M17 0,0279   | M3 0,0385    | M4 0,0463     | M14 0,0346   | M16 0,0389   | M11 0,0442   | C12 0,0494    | M15 0,0323   | M10 0,0362   | C3 0,0484    | M11 0,0520    | M15 0,0241   | M12 0,0244   | C8 0,0292    | M15 0,0319    |
| 26      | M4 0,0267    | C1 0,0281    | M17 0,0424   | M2 0,0485     | M16 0,0351   | M14 0,0390   | M8 0,0453    | M4 0,0495     | M4 0,0328    | M4 0,0366    | C1 0,0501    | C3 0,0538     | M14 0,0250   | M10 0,0247   | C11 0,0297   | M16 0,0320    |
| 27      | M5 0,0281    | M3 0,0313    | C3 0,0427    | M5 0,0539     | M11 0,0352   | M15 0,0394   | M17 0,0457   | M17 0,0515    | M6 0,0329    | M12 0,0370   | M12 0,0526   | M5 0,0539     | M8 0,0251    | M5 0,0248    | C18 0,0304   | C8 0,0321     |
| 28      | M15 0,0313   | M15 0,0315   | M2 0,0431    | M17 0,0563    | M7 0,0353    | M11 0,0402   | M14 0,0485   | M5 0,0537     | M3 0,0332    | M3 0,0374    | M7 0,0537    | M12 0,0557    | M10 0,0252   | M11 0,0261   | M11 0,0328   | M11 0,0343    |
| 29      | M16 0,0321   | M16 0,0317   | C1 0,0443    | M15 0,0575    | M15 0,0354   | M5 0,0412    | M16 0,0487   | M14 0,0546    | M12 0,0341   | M6 0,0381    | M6 0,0542    | C1 0,0570     | M11 0,0256   | M8 0,0274    | M8 0,0334    | M8 0,0367     |
| 30      | M3 0,0323    | M1 0,0338    | M15 0,0449   | M16 0,0576    | M8 0,0414    | M8 0,0466    | M15 0,0495   | M16 0,0562    | M7 0,0350    | M7 0,0401    | M3 0,0551    | M3 0,0578     | M13 0,0260   | M6 0,0283    | M6 0,0430    | M7 0,0502     |
| 31      | M9 0,0334    | M2 0,0344    | M16 0,0451   | M14 0,0583    | M13 0,0415   | M12 0,0528   | M12 0,0556   | M15 0,0564    | M5 0,0397    | M8 0,0420    | M4 0,0574    | M4 0,0677     | M7 0,0263    | M7 0,0314    | M7 0,0454    | M6 0,0505     |
| 32      | M2 0,0337    | M14 0,0347   | M14 0,0470   | C3 0,0852     | M12 0,0419   | C3 0,0944    | C3 0,1211    | C3 0,1318     | M8 0,0414    | M5 0,0456    | M5 0,0576    | M6 0,0698     | M6 0,0269    | C3 0,0821    | C3 0,1312    | C3 0,2110     |
| 33      | M1 0,0339    | M5 0,0448    | M5 0,0503    | C1 0,0923     | C3 0,1005    | C1 0,1039    | C1 0,1334    | C1 0,1450     | M13 0,0455   | C18 0,0612   | M9 0,0970    | M9 0,0836     | C3 0,1031    | C1 0,0911    | C1 0,1469    | C1 0,2360     |
| 34      | M14 0,0343   | M9 0,0717    | M9 0,0950    | M13 0,6647    | C1 0,1114    | M13 0,2298   | M13 0,6041   | M13 0,9579    | M9 0,0475    | M9 0,1052    | C18 0,1192   | C18 0,1209    | C1 0,1152    | M13 0,7218   | M9 1,1484    | M9 1,5881     |
| 35      | M13 0,0386   | M13 0,1648   | M13 0,4439   | M9 1,0902     | M9 1,7149    | M9 1,5379    | M9 1,8892    | M9 1,8908     | C18 0,0668   | M13 0,1734   | M13 0,4731   | M13 0,7258    | M9 1,8899    | M9 1,1161    | M13 1,9437   | M13 3,1870    |

**Table 5.3d: Forecasts of Industrial Production**

| Ranking | Japan |        |       |        |       |        |       |        | Luxembourg |        |       |        |       |        |       |        | The Netherlands |        |       |        |       |        |       |        | Portugal |        |       |        |       |        |      |        |
|---------|-------|--------|-------|--------|-------|--------|-------|--------|------------|--------|-------|--------|-------|--------|-------|--------|-----------------|--------|-------|--------|-------|--------|-------|--------|----------|--------|-------|--------|-------|--------|------|--------|
|         | h=1   |        | h=3   |        | h=8   |        | h=12  |        | h=1        |        | h=3   |        | h=8   |        | h=12  |        | h=1             |        | h=3   |        | h=8   |        | h=12  |        | h=1      |        | h=3   |        | h=8   |        | h=12 |        |
|         | RMSPE | RMSPE  | RMSPE | RMSPE  | RMSPE | RMSPE  | RMSPE | RMSPE  | RMSPE      | RMSPE  | RMSPE | RMSPE  | RMSPE | RMSPE  | RMSPE | RMSPE  | RMSPE           | RMSPE  | RMSPE | RMSPE  | RMSPE | RMSPE  | RMSPE | RMSPE  | RMSPE    | RMSPE  | RMSPE | RMSPE  | RMSPE | RMSPE  |      |        |
| 1       | M12   | 0,0192 | C2    | 0,0243 | M1    | 0,0360 | M7    | 0,0459 | M9         | 0,0331 | C15   | 0,0368 | M16   | 0,0414 | M16   | 0,0391 | M11             | 0,0216 | C2    | 0,0267 | M4    | 0,0284 | M4    | 0,0274 | M5       | 0,0496 | M4    | 0,0556 | M4    | 0,0617 | M12  | 0,0685 |
| 2       | C5    | 0,0193 | C11   | 0,0243 | C10   | 0,0384 | M1    | 0,0477 | C1         | 0,0348 | C4    | 0,0368 | M14   | 0,0423 | M1    | 0,0391 | C17             | 0,0216 | C13   | 0,0267 | M3    | 0,0295 | M3    | 0,0288 | M17      | 0,0505 | M1    | 0,0566 | M1    | 0,0623 | M11  | 0,0690 |
| 3       | C6    | 0,0193 | C5    | 0,0244 | C17   | 0,0393 | C17   | 0,0507 | C3         | 0,0350 | C14   | 0,0369 | M1    | 0,0426 | M17   | 0,0401 | C16             | 0,0216 | M11   | 0,0267 | M2    | 0,0307 | M2    | 0,0299 | M4       | 0,0505 | M11   | 0,0579 | M12   | 0,0630 | M8   | 0,0694 |
| 4       | C15   | 0,0193 | C6    | 0,0244 | C16   | 0,0393 | M6    | 0,0510 | C15        | 0,0355 | C16   | 0,0369 | C13   | 0,0437 | M14   | 0,0406 | C4              | 0,0217 | C12   | 0,0268 | C9    | 0,0313 | C14   | 0,0313 | C10      | 0,0509 | M12   | 0,0584 | M11   | 0,0645 | C18  | 0,0708 |
| 5       | C4    | 0,0193 | C4    | 0,0244 | C15   | 0,0394 | C16   | 0,0513 | C4         | 0,0355 | C9    | 0,0369 | M17   | 0,0439 | M15   | 0,0424 | C15             | 0,0217 | M3    | 0,0268 | C8    | 0,0317 | C9    | 0,0317 | C15      | 0,0512 | C10   | 0,0591 | C10   | 0,0652 | C8   | 0,0721 |
| 6       | C7    | 0,0193 | C15   | 0,0244 | C4    | 0,0394 | C6    | 0,0516 | C18        | 0,0356 | C5    | 0,0370 | M15   | 0,0439 | C17   | 0,0441 | C3              | 0,0217 | C9    | 0,0270 | M11   | 0,0317 | C17   | 0,0321 | C4       | 0,0512 | M17   | 0,0593 | C13   | 0,0659 | M4   | 0,0722 |
| 7       | C16   | 0,0193 | C14   | 0,0245 | C5    | 0,0397 | C5    | 0,0517 | C16        | 0,0357 | M16   | 0,0370 | C2    | 0,0440 | C13   | 0,0443 | C10             | 0,0217 | C8    | 0,0270 | C11   | 0,0318 | C16   | 0,0322 | C16      | 0,0512 | C4    | 0,0598 | C2    | 0,0659 | M7   | 0,0729 |
| 8       | C10   | 0,0193 | C16   | 0,0245 | C2    | 0,0399 | C10   | 0,0517 | C5         | 0,0357 | C6    | 0,0371 | C17   | 0,0442 | C10   | 0,0446 | C5              | 0,0218 | C14   | 0,0270 | C7    | 0,0318 | C12   | 0,0322 | C13      | 0,0513 | C15   | 0,0598 | C14   | 0,0661 | C9   | 0,0740 |
| 9       | C17   | 0,0193 | C7    | 0,0245 | C6    | 0,0399 | C7    | 0,0517 | C17        | 0,0357 | C17   | 0,0371 | M5    | 0,0445 | C16   | 0,0449 | C13             | 0,0218 | C7    | 0,0270 | C17   | 0,0319 | C7    | 0,0324 | C17      | 0,0513 | C17   | 0,0598 | C17   | 0,0661 | C11  | 0,0748 |
| 10      | C8    | 0,0194 | C17   | 0,0245 | C14   | 0,0400 | C4    | 0,0517 | C6         | 0,0358 | C10   | 0,0371 | C10   | 0,0445 | M5    | 0,0450 | C1              | 0,0218 | C6    | 0,0271 | C16   | 0,0319 | C4    | 0,0324 | C2       | 0,0514 | C16   | 0,0599 | C16   | 0,0662 | M1   | 0,0748 |
| 11      | C13   | 0,0195 | C9    | 0,0245 | C7    | 0,0405 | C15   | 0,0517 | C7         | 0,0360 | C7    | 0,0372 | C16   | 0,0448 | C4    | 0,0454 | C6              | 0,0218 | C5    | 0,0271 | C6    | 0,0319 | C15   | 0,0324 | C5       | 0,0514 | C5    | 0,0600 | C4    | 0,0662 | C2   | 0,0756 |
| 12      | C9    | 0,0195 | C8    | 0,0245 | M7    | 0,0405 | C14   | 0,0523 | C14        | 0,0360 | C3    | 0,0374 | C15   | 0,0453 | C15   | 0,0454 | C14             | 0,0219 | C15   | 0,0271 | C5    | 0,0320 | C6    | 0,0324 | C14      | 0,0516 | C6    | 0,0602 | C15   | 0,0662 | C14  | 0,0759 |
| 13      | M5    | 0,0196 | C10   | 0,0246 | C13   | 0,0408 | C9    | 0,0531 | C11        | 0,0366 | C2    | 0,0375 | C4    | 0,0453 | C14   | 0,0454 | C7              | 0,0219 | C4    | 0,0271 | C4    | 0,0320 | C5    | 0,0324 | C6       | 0,0517 | C13   | 0,0603 | C9    | 0,0665 | C12  | 0,0759 |
| 14      | M8    | 0,0196 | M8    | 0,0248 | M2    | 0,0413 | M2    | 0,0533 | C8         | 0,0369 | C12   | 0,0377 | C5    | 0,0454 | C8    | 0,0454 | C2              | 0,0220 | M1    | 0,0271 | C15   | 0,0320 | C10   | 0,0325 | M10      | 0,0519 | C2    | 0,0605 | C5    | 0,0665 | C7   | 0,0766 |
| 15      | M17   | 0,0197 | M11   | 0,0248 | C9    | 0,0427 | C8    | 0,0538 | C10        | 0,0373 | C11   | 0,0378 | C6    | 0,0455 | C11   | 0,0455 | C9              | 0,0223 | C16   | 0,0271 | C12   | 0,0321 | C2    | 0,0326 | C7       | 0,0520 | C7    | 0,0607 | C6    | 0,0668 | C6   | 0,0768 |
| 16      | C11   | 0,0197 | C13   | 0,0249 | M6    | 0,0430 | C12   | 0,0541 | C12        | 0,0375 | C1    | 0,0379 | C7    | 0,0458 | C5    | 0,0455 | C12             | 0,0223 | M4    | 0,0272 | C14   | 0,0322 | M16   | 0,0327 | M6       | 0,0527 | C14   | 0,0608 | M8    | 0,0673 | C5   | 0,0769 |
| 17      | C2    | 0,0197 | C12   | 0,0251 | C8    | 0,0436 | C11   | 0,0544 | C2         | 0,0376 | C13   | 0,0379 | C14   | 0,0458 | C6    | 0,0456 | C8              | 0,0225 | C17   | 0,0272 | C10   | 0,0322 | C13   | 0,0329 | C9       | 0,0534 | M7    | 0,0610 | C7    | 0,0673 | C4   | 0,0770 |
| 18      | C12   | 0,0197 | M12   | 0,0252 | C11   | 0,0442 | C2    | 0,0549 | C13        | 0,0377 | C8    | 0,0384 | C8    | 0,0468 | C2    | 0,0458 | M4              | 0,0231 | C10   | 0,0272 | C13   | 0,0322 | C18   | 0,0334 | M7       | 0,0537 | M6    | 0,0619 | C12   | 0,0683 | C15  | 0,0770 |
| 19      | M6    | 0,0200 | M7    | 0,0252 | C12   | 0,0443 | C13   | 0,0563 | C9         | 0,0378 | M14   | 0,0387 | C18   | 0,0468 | C7    | 0,0459 | C11             | 0,0232 | M2    | 0,0276 | C2    | 0,0325 | M15   | 0,0337 | C8       | 0,0539 | C8    | 0,0624 | C18   | 0,0689 | C17  | 0,0770 |
| 20      | M11   | 0,0201 | M6    | 0,0264 | M8    | 0,0464 | M8    | 0,0571 | M16        | 0,0381 | M1    | 0,0393 | M2    | 0,0469 | C12   | 0,0466 | M10             | 0,0233 | C11   | 0,0276 | M16   | 0,0332 | C8    | 0,0338 | M12      | 0,0541 | C9    | 0,0627 | M7    | 0,0699 | C16  | 0,0770 |
| 21      | C18   | 0,0201 | M4    | 0,0266 | M14   | 0,0469 | M4    | 0,0576 | M14        | 0,0384 | M3    | 0,0395 | M3    | 0,0469 | M10   | 0,0467 | M1              | 0,0233 | M17   | 0,0287 | M7    | 0,0336 | C11   | 0,0341 | C12      | 0,0557 | C18   | 0,0628 | M17   | 0,0709 | C10  | 0,0783 |
| 22      | C14   | 0,0203 | M17   | 0,0266 | M4    | 0,0474 | M3    | 0,0594 | M2         | 0,0385 | M2    | 0,0399 | C9    | 0,0473 | C9    | 0,0476 | M17             | 0,0234 | M16   | 0,0289 | M15   | 0,0340 | M11   | 0,0346 | M11      | 0,0560 | C12   | 0,0641 | C11   | 0,0715 | M6   | 0,0802 |
| 23      | M4    | 0,0204 | C18   | 0,0282 | M11   | 0,0477 | M14   | 0,0649 | M1         | 0,0385 | M15   | 0,0402 | C12   | 0,0478 | M2    | 0,0487 | M2              | 0,0234 | M15   | 0,0290 | M12   | 0,0344 | M7    | 0,0348 | M1       | 0,0561 | M10   | 0,0641 | M3    | 0,0725 | C13  | 0,0810 |
| 24      | M7    | 0,0209 | M2    | 0,0284 | C18   | 0,0493 | M5    | 0,0678 | M15        | 0,0389 | M5    | 0,0406 | M10   | 0,0485 | M3    | 0,0503 | M12             | 0,0237 | C3    | 0,0293 | M17   | 0,0344 | M1    | 0,0355 | M2       | 0,0567 | M8    | 0,0650 | M2    | 0,0727 | M3   | 0,0821 |
| 25      | M10   | 0,0213 | C3    | 0,0285 | M5    | 0,0502 | M17   | 0,0693 | M3         | 0,0394 | C18   | 0,0423 | C11   | 0,0499 | C18   | 0,0507 | M3              | 0,0237 | M10   | 0,0298 | M1    | 0,0347 | M17   | 0,0356 | C11      | 0,0571 | C11   | 0,0654 | M6    | 0,0729 | M2   | 0,0822 |
| 26      | M2    | 0,0228 | M1    | 0,0292 | M17   | 0,0514 | M10   | 0,0706 | M17        | 0,0397 | M17   | 0,0423 | M4    | 0,0516 | M8    | 0,0530 | M7              | 0,0237 | C1    | 0,0299 | M10   | 0,0350 | M10   | 0,0357 | M3       | 0,0577 | M2    | 0,0656 | C8    | 0,0730 | M10  | 0,0864 |
| 27      | M3    | 0,0230 | M10   | 0,0294 | M12   | 0,0525 | C18   | 0,0753 | M4         | 0,0401 | M10   | 0,0423 | M8    | 0,0517 | M11   | 0,0531 | M16             | 0,0238 | M14   | 0,0309 | M8    | 0,0358 | M12   | 0,0366 | C18      | 0,0581 | M3    | 0,0660 | M10   | 0,0746 | M17  | 0,0886 |
| 28      | M14   | 0,0232 | C1    | 0,0294 | M3    | 0,0535 | M11   | 0,0766 | M10        | 0,0402 | M4    | 0,0426 | M11   | 0,0535 | M12   | 0,0534 | M15             | 0,0240 | M12   | 0,0311 | C18   | 0,0363 | M8    | 0,0387 | M15      | 0,0581 | M14   | 0,0678 | M16   | 0,0772 | M5   | 0,0931 |
| 29      | M15   | 0,0236 | M14   | 0,0299 | M10   | 0,0540 | M16   | 0,0788 | M6         | 0,0408 | M12   | 0,0434 | M12   | 0,0541 | M4    | 0,0543 | C18             | 0,0240 | C18   | 0,0313 | M6    | 0,0389 | M6    | 0,0406 | M14      | 0,0584 | M15   | 0,0678 | M5    | 0,0779 | M14  | 0,0939 |
| 30      | M16   | 0,0240 | M5    | 0,0300 | M16   | 0,0557 | M12   | 0,0807 | M12        | 0,0435 | M11   | 0,0437 | M6    | 0,0567 | M7    | 0,0608 | M14             | 0,0248 | M7    | 0,0318 | M14   | 0,0411 | M14   | 0,0419 | M8       | 0,0589 | M5    | 0,0688 | M15   | 0,0780 | M15  | 0,0942 |
| 31      | M1    | 0,0259 | M3    | 0,0302 | M15   | 0,0575 | M15   | 0,0813 | M8         | 0,0435 | M6    | 0,0442 | M7    | 0,0579 | M6    | 0,0619 | M5              | 0,0251 | M6    | 0,0333 | M5    | 0,0437 | M5    | 0,0457 | M16      | 0,0602 | M16   | 0,0706 | M14   | 0,0781 | M16  | 0,1005 |
| 32      | M13   | 0,0309 | M15   | 0,0320 | C3    | 0,0618 | C3    | 0,0932 | M11        | 0,0445 | M8    | 0,0448 | C3    | 0,0672 | C3    | 0,0805 | M6              | 0,0253 | M5    | 0,0338 | C3    | 0,0922 | C3    | 0,0772 | M13      | 0,0929 | C3    | 0,0992 | C3    | 0,1246 | C3   | 0,1426 |
| 33      | C3    | 0,0669 | M16   | 0,0323 | C1    | 0,0663 | C1    | 0,1000 | M5         | 0,0458 | M7    | 0,0491 | C1    | 0,0717 | C1    | 0,0878 | M8              | 0,0263 | M8    | 0,0344 | C1    | 0,1016 |       |        |          |        |       |        |       |        |      |        |

**Table 5.3e:** Forecasts of Industrial Production

| Ranking | Sweden |        |     |        |     |        |      |        | USA |        |     |        |     |        |      |        |
|---------|--------|--------|-----|--------|-----|--------|------|--------|-----|--------|-----|--------|-----|--------|------|--------|
|         | h=1    |        | h=3 |        | h=8 |        | h=12 |        | h=1 |        | h=3 |        | h=8 |        | h=12 |        |
|         |        | RMSPE  |     | RMSPE  |     | RMSPE  |      | RMSPE  |     | RMSPE  |     | RMSPE  |     | RMSPE  |      | RMSPE  |
| 1       | M11    | 0,0361 | M12 | 0,0447 | M6  | 0,0564 | M6   | 0,0568 | C11 | 0,0085 | M6  | 0,0134 | M11 | 0,0288 | C11  | 0,0323 |
| 2       | C1     | 0,0365 | M11 | 0,0454 | M7  | 0,0608 | M7   | 0,0592 | M6  | 0,0085 | M7  | 0,0135 | C8  | 0,0289 | M1   | 0,0352 |
| 3       | C3     | 0,0366 | M6  | 0,0459 | M12 | 0,0641 | M8   | 0,0665 | C8  | 0,0085 | C11 | 0,0135 | M7  | 0,0292 | M7   | 0,0356 |
| 4       | C17    | 0,0371 | M7  | 0,0464 | M8  | 0,0669 | M12  | 0,0696 | C9  | 0,0086 | M10 | 0,0136 | M1  | 0,0294 | M11  | 0,0364 |
| 5       | M12    | 0,0372 | C17 | 0,0468 | C10 | 0,0689 | C8   | 0,0721 | C2  | 0,0086 | M11 | 0,0138 | C11 | 0,0298 | C12  | 0,0377 |
| 6       | M6     | 0,0373 | C16 | 0,0471 | C16 | 0,0692 | M10  | 0,0743 | C14 | 0,0086 | C8  | 0,0139 | C14 | 0,0307 | C2   | 0,0381 |
| 7       | C16    | 0,0373 | C4  | 0,0474 | C4  | 0,0692 | C18  | 0,0761 | C13 | 0,0086 | C9  | 0,0139 | C12 | 0,0307 | C13  | 0,0381 |
| 8       | C15    | 0,0375 | C15 | 0,0474 | C15 | 0,0692 | C2   | 0,0764 | M1  | 0,0086 | C14 | 0,0140 | C9  | 0,0309 | C14  | 0,0387 |
| 9       | C4     | 0,0375 | C5  | 0,0475 | C17 | 0,0693 | M4   | 0,0765 | C3  | 0,0086 | C12 | 0,0140 | C7  | 0,0313 | M8   | 0,0389 |
| 10      | C14    | 0,0376 | C14 | 0,0476 | C5  | 0,0695 | C11  | 0,0766 | C12 | 0,0086 | C13 | 0,0141 | C2  | 0,0313 | M3   | 0,0397 |
| 11      | C10    | 0,0377 | C10 | 0,0476 | C6  | 0,0697 | C15  | 0,0766 | C1  | 0,0086 | C2  | 0,0142 | M8  | 0,0314 | M12  | 0,0403 |
| 12      | C5     | 0,0377 | C6  | 0,0476 | M10 | 0,0699 | C4   | 0,0766 | C7  | 0,0087 | C7  | 0,0142 | C17 | 0,0316 | M2   | 0,0410 |
| 13      | C6     | 0,0378 | C7  | 0,0478 | C2  | 0,0700 | C16  | 0,0767 | C17 | 0,0087 | C6  | 0,0143 | C6  | 0,0316 | M10  | 0,0432 |
| 14      | C7     | 0,0380 | C2  | 0,0483 | C7  | 0,0701 | C17  | 0,0767 | C16 | 0,0087 | C5  | 0,0143 | M12 | 0,0317 | M15  | 0,0459 |
| 15      | C2     | 0,0382 | C9  | 0,0486 | C14 | 0,0705 | C5   | 0,0767 | C6  | 0,0087 | C15 | 0,0144 | C5  | 0,0318 | M6   | 0,0473 |
| 16      | C13    | 0,0385 | C13 | 0,0489 | M4  | 0,0705 | C10  | 0,0769 | C4  | 0,0087 | C4  | 0,0144 | C16 | 0,0318 | M5   | 0,0475 |
| 17      | M2     | 0,0385 | C12 | 0,0494 | M3  | 0,0710 | M3   | 0,0769 | C15 | 0,0087 | C16 | 0,0144 | C13 | 0,0318 | M17  | 0,0491 |
| 18      | M3     | 0,0386 | M3  | 0,0497 | C11 | 0,0711 | C6   | 0,0769 | C5  | 0,0087 | C10 | 0,0144 | M10 | 0,0320 | M4   | 0,0509 |
| 19      | C8     | 0,0387 | C11 | 0,0497 | M2  | 0,0712 | C7   | 0,0771 | C10 | 0,0087 | M1  | 0,0144 | C4  | 0,0320 | M14  | 0,0543 |
| 20      | C11    | 0,0387 | M2  | 0,0497 | C13 | 0,0712 | M2   | 0,0771 | M11 | 0,0089 | C17 | 0,0145 | C15 | 0,0320 | M16  | 0,0544 |
| 21      | C9     | 0,0388 | C8  | 0,0499 | C18 | 0,0713 | C14  | 0,0781 | M7  | 0,0089 | C3  | 0,0147 | C10 | 0,0322 | C3   | 0,0601 |
| 22      | C12    | 0,0390 | M4  | 0,0502 | C9  | 0,0719 | C13  | 0,0789 | M10 | 0,0089 | C1  | 0,0147 | M6  | 0,0348 | C10  | 0,0636 |
| 23      | M7     | 0,0392 | M5  | 0,0504 | C8  | 0,0720 | C9   | 0,0803 | M17 | 0,0090 | M8  | 0,0149 | C3  | 0,0350 | C1   | 0,0641 |
| 24      | M4     | 0,0394 | M17 | 0,0505 | C12 | 0,0726 | C12  | 0,0835 | M12 | 0,0092 | M12 | 0,0151 | C1  | 0,0352 | C4   | 0,0681 |
| 25      | M17    | 0,0398 | C3  | 0,0508 | M11 | 0,0726 | M11  | 0,0844 | C18 | 0,0093 | C18 | 0,0159 | C18 | 0,0357 | C15  | 0,0681 |
| 26      | M14    | 0,0398 | C1  | 0,0519 | M5  | 0,0728 | M5   | 0,0864 | M4  | 0,0094 | M17 | 0,0163 | M3  | 0,0362 | C5   | 0,0708 |
| 27      | M16    | 0,0399 | M16 | 0,0522 | M17 | 0,0779 | M17  | 0,0908 | M8  | 0,0097 | M4  | 0,0171 | M9  | 0,0372 | C6   | 0,0737 |
| 28      | M15    | 0,0401 | M14 | 0,0525 | M16 | 0,0791 | M14  | 0,0912 | M16 | 0,0099 | M16 | 0,0178 | M2  | 0,0372 | C16  | 0,0754 |
| 29      | M1     | 0,0403 | M1  | 0,0530 | M14 | 0,0792 | M16  | 0,0913 | M15 | 0,0102 | M15 | 0,0178 | M17 | 0,0388 | C17  | 0,0791 |
| 30      | M10    | 0,0406 | C18 | 0,0531 | M15 | 0,0798 | M15  | 0,0915 | M14 | 0,0108 | M3  | 0,0190 | M15 | 0,0392 | C7   | 0,0795 |
| 31      | C18    | 0,0417 | M15 | 0,0534 | M1  | 0,0810 | M1   | 0,0928 | M3  | 0,0108 | M14 | 0,0192 | M5  | 0,0419 | C9   | 0,0859 |
| 32      | M5     | 0,0438 | M8  | 0,0535 | C3  | 0,1065 | C3   | 0,1375 | M2  | 0,0109 | M2  | 0,0194 | M4  | 0,0425 | C8   | 0,1529 |
| 33      | M8     | 0,0455 | M10 | 0,0539 | C1  | 0,1126 | C1   | 0,1474 | M13 | 0,0114 | M5  | 0,0205 | M16 | 0,0433 | M13  | 0,2470 |
| 34      | M9     | 0,0612 | M9  | 0,1834 | M9  | 0,8138 | M9   | 1,1111 | M9  | 0,0140 | M9  | 0,0239 | M14 | 0,0444 | C18  | 0,5860 |
| 35      | M13    | 0,0791 | M13 | 0,3021 | M13 | 0,8378 | M13  | 1,3664 | M5  | 0,0147 | M13 | 0,0524 | M13 | 0,1552 | M9   | 0,7627 |

**Table 5.4:** Average Ranking and Average RMSPE scaled by the RMSPE of M1

| Model | h=1     |       |        | h=3     |       |        | h=8     |       |        | h=12    |       |        |
|-------|---------|-------|--------|---------|-------|--------|---------|-------|--------|---------|-------|--------|
|       | Ranking | RMSPE | A/M1   |
| M1    | 23,2    | 0,031 | 1,000  | 18,2    | 0,036 | 1,000  | 15,1    | 0,048 | 1,000  | 14,8    | 0,053 | 1,000  |
| M2    | 24,6    | 0,031 | 1,014  | 24,4    | 0,037 | 1,055  | 20,1    | 0,049 | 1,053  | 17,5    | 0,053 | 1,031  |
| M3    | 25,2    | 0,031 | 1,017  | 22,4    | 0,037 | 1,047  | 20,3    | 0,050 | 1,076  | 17,8    | 0,054 | 1,049  |
| M4    | 19,6    | 0,029 | 0,948  | 20,2    | 0,036 | 1,000  | 19,7    | 0,050 | 1,077  | 18,3    | 0,055 | 1,098  |
| M5    | 23,2    | 0,032 | 1,048  | 30,1    | 0,041 | 1,178  | 28,6    | 0,056 | 1,202  | 26,1    | 0,062 | 1,192  |
| M6    | 20,6    | 0,030 | 0,972  | 20,9    | 0,038 | 1,030  | 20,2    | 0,052 | 1,111  | 18,8    | 0,058 | 1,164  |
| M7    | 25,1    | 0,032 | 1,010  | 17,8    | 0,038 | 1,028  | 16,8    | 0,049 | 1,069  | 14,4    | 0,052 | 1,041  |
| M8    | 29,0    | 0,034 | 1,092  | 27,4    | 0,041 | 1,119  | 20,4    | 0,050 | 1,062  | 14,4    | 0,051 | 0,999  |
| M9    | 33,4    | 0,772 | 28,034 | 35,4    | 0,652 | 20,096 | 35,1    | 0,927 | 20,877 | 35,4    | 1,101 | 23,707 |
| M10   | 21,3    | 0,030 | 0,965  | 22,6    | 0,037 | 1,028  | 20,2    | 0,050 | 1,078  | 20,2    | 0,057 | 1,094  |
| M11   | 17,9    | 0,030 | 0,964  | 16,2    | 0,036 | 0,991  | 17,4    | 0,049 | 1,043  | 17,4    | 0,055 | 1,057  |
| M12   | 19,4    | 0,030 | 0,979  | 17,3    | 0,036 | 1,012  | 16,9    | 0,049 | 1,050  | 15,7    | 0,055 | 1,062  |
| M13   | 33,8    | 0,047 | 1,464  | 35,6    | 0,259 | 8,741  | 35,5    | 0,724 | 18,990 | 35,4    | 1,154 | 28,311 |
| M14   | 28,1    | 0,032 | 1,035  | 27,1    | 0,039 | 1,082  | 26,7    | 0,054 | 1,152  | 25,9    | 0,062 | 1,189  |
| M15   | 27,5    | 0,032 | 1,026  | 27,7    | 0,039 | 1,087  | 27,5    | 0,055 | 1,186  | 26,7    | 0,063 | 1,241  |
| M16   | 27,2    | 0,032 | 1,025  | 25,6    | 0,038 | 1,077  | 26,5    | 0,054 | 1,176  | 26,2    | 0,063 | 1,236  |
| M17   | 17,6    | 0,029 | 0,939  | 18,7    | 0,035 | 0,985  | 21,9    | 0,050 | 1,079  | 22,4    | 0,058 | 1,127  |
| C1    | 21,2    | 0,062 | 2,205  | 29,2    | 0,062 | 1,874  | 32,3    | 0,097 | 2,273  | 33,1    | 0,123 | 2,785  |
| C2    | 15,8    | 0,029 | 0,924  | 12,8    | 0,034 | 0,951  | 14,4    | 0,047 | 0,988  | 14,7    | 0,052 | 0,990  |
| C3    | 19,9    | 0,058 | 2,033  | 27,7    | 0,058 | 1,743  | 31,1    | 0,090 | 2,096  | 31,8    | 0,113 | 2,545  |
| C4    | 9,3     | 0,028 | 0,906  | 8,3     | 0,034 | 0,933  | 9,3     | 0,046 | 0,968  | 12,2    | 0,053 | 1,023  |
| C5    | 10,4    | 0,028 | 0,906  | 8,8     | 0,034 | 0,934  | 9,7     | 0,046 | 0,969  | 12,3    | 0,053 | 1,027  |
| C6    | 10,9    | 0,028 | 0,906  | 9,4     | 0,034 | 0,935  | 10,1    | 0,046 | 0,969  | 12,1    | 0,053 | 1,031  |
| C7    | 10,8    | 0,028 | 0,906  | 10,6    | 0,034 | 0,936  | 10,6    | 0,046 | 0,971  | 12,1    | 0,053 | 1,041  |
| C8    | 10,4    | 0,028 | 0,909  | 11,8    | 0,034 | 0,940  | 13,8    | 0,047 | 0,992  | 11,9    | 0,057 | 1,165  |
| C9    | 13,8    | 0,029 | 0,919  | 12,3    | 0,034 | 0,944  | 12,4    | 0,047 | 0,982  | 13,8    | 0,054 | 1,059  |
| C10   | 9,9     | 0,028 | 0,904  | 9,7     | 0,034 | 0,934  | 9,3     | 0,046 | 0,966  | 12,8    | 0,053 | 1,017  |
| C11   | 12,9    | 0,029 | 0,916  | 12,7    | 0,035 | 0,944  | 15,7    | 0,048 | 1,010  | 14,4    | 0,052 | 0,987  |
| C12   | 17,1    | 0,029 | 0,929  | 15,1    | 0,035 | 0,957  | 17,2    | 0,048 | 1,002  | 14,2    | 0,053 | 0,993  |
| C13   | 13,9    | 0,029 | 0,918  | 13,9    | 0,034 | 0,951  | 15,7    | 0,047 | 0,991  | 16,9    | 0,053 | 0,999  |
| C14   | 12,3    | 0,028 | 0,912  | 11,2    | 0,034 | 0,938  | 11,7    | 0,047 | 0,975  | 12,9    | 0,051 | 0,982  |
| C15   | 9,3     | 0,028 | 0,906  | 8,2     | 0,034 | 0,933  | 9,6     | 0,046 | 0,968  | 12,6    | 0,053 | 1,023  |
| C16   | 9,3     | 0,028 | 0,904  | 9,4     | 0,034 | 0,934  | 9,1     | 0,046 | 0,968  | 12,1    | 0,053 | 1,035  |
| C17   | 9,0     | 0,028 | 0,904  | 10,8    | 0,034 | 0,935  | 9,3     | 0,046 | 0,968  | 12,0    | 0,053 | 1,040  |
| C18   | 21,6    | 0,032 | 1,025  | 23,7    | 0,039 | 1,090  | 21,9    | 0,058 | 1,255  | 19,6    | 0,096 | 2,253  |

**Note:** A/M1 denotes the Average RMSPE of Models i, scaled by the RMSPE of M1